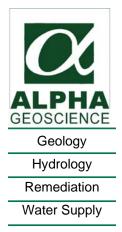
HYDROGEOLOGIC ANALYSIS OF THE PROPOSED EXPANSION OF THE HANSON AGGREGATES NEW YORK LLC HONEOYE FALLS QUARRY

Prepared for:

Hanson Aggregates New York LLC 4800 Jamesville Rd, PO Box 513 Jamesville, New York 13078



April 1, 2013



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1.0 INTRODUCTION

This report was prepared by Alpha Geoscience (Alpha) and presents a hydrogeologic analysis of the proposed expansion area for the Honeoye Falls limestone aggregate rock quarry. The quarry is owned and operated by Hanson Aggregates New York LLC (Hanson) and is currently located in the Towns of Lima and Avon, Livingston County, and in the Towns of Honeoye Falls and Mendon, Monroe County (Figure 1). Hanson is considering expanding the existing mining operation westward from the existing western permitted life-of-mine boundary. The majority of the expansion area will be located within the Town of Rush, with a relatively small portion within the Town of Avon.

The objectives of the hydrogeologic evaluation were to provide information about the physical characteristics of the ground water system within and around the expansion area, describe the anticipated changes that will occur to that ground water system when the mine is at its currently proposed maximum extent, evaluate the potential impacts to neighboring residential wells and an adjacent wetland, and evaluate the adequacy of the present sump location to continue to serve the mine as expansion progresses.

2.0 METHODS

The evaluation objectives were met through a series of tasks that included:

- a literature review;
- site inspection;
- rock core and drill cuttings inspection;
- shallow piezometer installation;
- water level measurements; and
- hydrogeologic analysis.

2.1 Literature Review

Published and unpublished information was obtained and reviewed to assess the general conditions of the local and regional ground water systems in the context of the proposed mine expansion. A FOIL request was made to the NYSDEC for well completion reports filed since Alpha's last such FOIL request for the area in 2009. FOIL requests were also made to the Monroe County Department of Health and to Livingston County for available databases on well logs, well reports and water levels in the area of Hanson's Honeoye Falls quarry. The NYSDEC well completion reports for the residential wells are included in Appendix A. The FOIL requests to Monroe and Livingston Counties yielded no new information.

2.2 Site Inspection

The site was inspected by Mr. Steven Trader of Alpha on April 8, 2011. Mr. Trader observed the sump, the water handling system, and the occurrence of water in the floor and highwall of the existing quarry. Dr. Samuel Gowan of Alpha conducted a similar inspection of the mine in 2003.

Mr. Trader and Mr. Michael Lewis, Hanson's Environmental Manager, observed the measurement of water levels from the site wells, sump and local culverts by Mr. Larry Clark, Honeoye Falls mine Superintendent. Mr. Clark has been the Hanson representative primarily responsible for performing the water level measurements at the site since 2009.

2.3 Rock Core and Cuttings Inspection

Hanson, in 1998 and 2002, drilled the following bedrock core holes in the vicinity of the expansion area: DDH 4-98, DDH 5-98, DDH 1-02, DDH 2-02, and DDH 4-02. The depths of the core holes ranged from 123 ft to 139 ft. The uppermost bedrock formation encountered in each of the core holes was limestone of the Onondaga Formation (Fm). Each of the core holes were advanced through the Onondaga limestone and into the top of the Akron Fm, which is the upper member of the Bertie Group (Salina Group) and is not mined at the quarry. The locations of the core holes are shown on Figure 2.

Geologic characteristics of the rock cores were logged previously by others and are not presented herein. Alpha personnel inspected the rock core from four of these holes (all except DDH 2-02) on April 7 and 8, 2011 at the Honeoye Falls Quarry office. The rock cores were inspected by Alpha to specifically look at fractures. The depth and physical characteristics of all core breaks that appeared to represent natural, water-bearing fractures were recorded (Appendix B). Fractures created by the coring process were either indicated as such or were not recorded.

Hanson installed five monitoring wells in the vicinity of the expansion area during 2009 (09-001, 09-002, 09-003) and 2010 (10-001, 10-002). The driller filed well completion reports for the NYSDEC for the 2009 wells and provided drilling logs for all five wells. The 2009 logs also included observations and notes made by Hanson personnel. The logs for the expansion area wells are included in Appendix C. Hanson saved cuttings from the 2009 and 2010 wells at intervals of approximately 5 ft. The cuttings from the 2009 wells were inspected by Alpha to evaluate the presence of the Onondaga/Akron contact for stratigraphic control. Results of the cuttings inspection are included on the logs for the 2009 wells in Appendix C.

2.4 Shallow Piezometer Installation

A shallow piezometer was installed by Alpha within the delineated wetland on the southwest side of the expansion area at a location where no surface water was apparent on April 20, 2011 (Figure 2). The purpose of the piezometer (P-1) was to assist in the evaluation of the potential effect of the quarry expansion on the wetland. P-1 also allowed for measurement of water levels within the unconsolidated materials above bedrock, and to allow a comparison of those levels with the elevation of the bedrock potentiometric surface. P-1 was installed by hand using a power auger to drill a six-inch diameter hole to refusal at 32 inches below grade. Three additional holes were attempted in the vicinity off the final P-1 location and each met refusal at approximately 32 inches below grade; consequently, refusal was likely the top of bedrock. The well construction log and geologic log of P-1 are included in Appendix D. The elevation of P-1 was surveyed by Alpha relative to existing, previously surveyed, wells. The location of P-1 was measured via GPS.

2.5 Water Level Measurements

Water level data were analyzed to determine existing ground water flow patterns, assess the influence of quarry pump-out on the water table in the expansion area, and evaluate the potential impact to nearby residential wells and the nearby wetland. Data collected by Hanson include water levels from the sump, 15 wells in and around the quarry, three residential wells, wetland piezometer P1, and culverts in the intermittent stream, which drains the wetland on the southwest of the expansion area. Water level measurements in most of the wells have been recorded on an approximately weekly basis since August 20, 2009 (Plate 1). Prior to that time, water levels were recorded on an intermittent basis.

2.6 Hydrogeologic Analysis

All the data were analyzed to develop an understanding of the ground water and surface water systems and evaluate how they will be affected by mining in the proposed expansion area. A ground water contour map was constructed to represent the existing ground water elevations, flow directions, and local ground water divides during the seasonal low water level conditions. It is during seasonal low water level conditions when nearby residential wells potentially would be most vulnerable to water level decline due to quarry expansion and dewatering.

A structural contour map of the contact between the Onondaga Fm and the Akron Fm was constructed based on the geologic logs of the core holes penetrating the Akron Formation at the quarry provided by Hanson. The general mining plan by Hanson is to mine the Onondaga limestone down to approximately the top of the Akron Fm and maintain a downward slope to the south and east.

The ground water contours and the top-of-Akron structure contours were used to create three hydrogeologic cross sections for the expansion area. Knowledge of the aquifer system was combined with Hanson's proposed mining plan to represent future conditions on the hydrogeologic cross sections. The hydrogeologic cross sections illustrate the relative change in ground water levels between the existing and future conditions and show the extent of drawdown

laterally from the quarry edge when the mine is at its greatest depth and lateral extent. This allowed for an evaluation of the potential impact to the nearby residential wells.

The recharge area for the wetland southwest of the expansion area includes a portion of the area to be mined; consequently, an evaluation of the potential impact on the wetland southwest of the expansion area was performed. The evaluation was based on water level data, the composition of the surficial deposits, and a recharge basin analysis.

3.0 **RESULTS**

3.1 Geology

3.1.2 Bedrock

The limestone of the Onondaga Fm is the primary unit being mined at the quarry and is the bedrock formation exposed at the surface or subcropping beneath unconsolidated sediments. The Onondaga formation is underlain by the limestones and dolostones of the Bertie Group. The uppermost unit of the Bertie Group at the site is the Akron Fm. The Akron Fm is exposed in the base of the quarry sump on the east side of the quarry (Spectra, 2000) and is penetrated by numerous wells and core holes at the site.

Elevation contours for the top of the Akron Fm are provided on Figure 4. The depth to the top of Akron was obtained from the core logs of the core holes Hanson has drilled at the site, the cuttings inspection of the 2009 series wells, and from well completion reports filed with the NYSDEC for nearby residential wells. The elevation contours on Figure 4 indicate that the top of Akron Fm surface has a local high area north of the existing western extension of the active quarry. The top of Akron fm surface slopes to the west, south and east from this relative high spot.

The shale units of the Marcellus Fm subcrop south of the quarry, generally above a surface elevation of approximately 710 ft above mean sea level (amsl), but these are not present within

the subsurface in the expansion area. Regionally, the bedrock formations all dip less than 1° to the south (Rickard and Fisher, 1978).

3.1.2 Surficial Deposits

The unconsolidated sediments above the Onondaga Fm in the proposed expansion area are approximately 1.5 to 15 feet thick based on the core logs and drilling logs provided by Hanson. The surficial deposits thicken toward the southwest and are up to 21 ft thick at DDH 4-02, which is located approximately 1,000 feet southwest of the expansion area (Figure 2). The surficial geology (sediments) over most of the site has been mapped as primarily consisting of glacial till (Muller and Cadwell, 1986). This is consistent with the fact that much of the soil surrounding the existing quarry site is mapped as moderately well drained Honeoye silt loam, which is derived from drumlins and till plains (National Resource Conservation Service, Online Web Soil Surveys). The soil surveys for Monroe and Livingston Counties also indicate that there is an area of very poorly drained silt loam in a shallow depression southwest of the expansion area (Figure 3). These areas are represented on Figure 3 by the Lyons (Lo), Colwoon (C8), Canandaigua (Ca) and Toledo (Tb) silt loams. These soils are derived from glaciolacustrine deposits and can be clayey, or have clayey horizons. This is consistent with the cuttings from the installation of piezometer P1 (Appendix D). Clay and silt of medium plasticity were the primary constituents of the P1 cuttings to approximately 2.7 ft below grade.

3.2 Hydrogeology

The hydrogeology of the expansion area is comprised of shallow, perched ground water and the bedrock aquifer. The following two sections will describe each of these in turn.

3.2.1 Perched Ground Water

The surface water system in the vicinity of the proposed expansion area is primarily comprised of a wetland southwest of, and adjacent to, the expansion area. It also includes the streams and ditches that lead through the wetland, as well as the saturated soils above bedrock in that area. The clayey nature of these soils (discussed in the previous section) impedes downward percolation to the bedrock aquifer; consequently, the shallow ground water within the unconsolidated sediments is perched and a wetland has developed in this low area. The wetland is generally present below an elevation of approximately 705 ft amsl.

Water is more able to percolate downward and infiltrate to the bedrock aquifer system outside of the wetland area and within the moderately well drained, till-derived soils. The elevation of the surface water system is distinctly higher than the bedrock aquifer (approximately 50 to 100 ft vertical separation; Plate 1) and is consistent with a perched ground water system. The one exception to this vertical separation is the water level at 10-002, which was at approximately the same elevation as at P1 for a portion of the time P1 had water. Water was encountered in bedrock at a depth of 15 ft during the drilling of well 10-002. Well 10-002 is located outside of the wetland area soils. The water level has fluctuated seasonally in 10-002 by up to 47 ft. It is possible that the northward flowing bedrock aquifer, south of the wetland, discharges seasonally to the wetland during spring high water conditions. This is not the case on the northern side of the wetland.

The water level elevations measured at shallow piezometer P1 were approximately three feet higher than the elevation of the wetland stream at the outlet. This difference is consistent with the shallow, perched, ground water flow discharging to the stream that runs through the wetland. The piezometer (P1) and the stream outlet at the culvert on Oak Openings Rd went dry at approximately the same time in late June 2011. The flow out of the wetland is ephemeral, despite elevated rainfall in the spring of 2011. The stream is likely a losing stream during the dry season, losing water along its course to the perched ground water system.

3.2.2 Bedrock Aquifer

Ground water within the bedrock in the region surrounding the quarry, apart from perched ground water, is contained within, and flows along, fractures, bedding plane partings, fault zones and dissolution-widened openings in the rock. The ground water intersected by the quarry occurs in the water table, which generally is in the top 150 feet of the rock.

Ground water flows from areas of high hydraulic head in the recharge areas toward the lower hydraulic head in the discharge zones. The rate that the ground water flows and the quantity of water contained within a unit volume of rock (storage) depends upon the width and number of fractures and dissolution-widened openings. Limestone bedrock, such as the Onondaga Fm, generally has greater fracture widths and, in many instances, can have dissolution-widened openings that can form significant ground water flow paths, especially in karst terrain. Wells installed in karst terrain are often susceptible to large fluctuations in water levels, especially during droughty periods. Karst features have been identified in the region surrounding the quarry; however, site inspections by Alpha personnel indicated that karst features identified in the region are not visible in the quarry. Ground water flows into the quarry via nearly vertical joints and horizontal bedding plane partings that are visible in the quarry face.

Knowledge of the bedrock aquifer in the immediate vicinity of the quarry and the expansion area comes from the driller's logs of the monitoring wells installed by Hanson, drillers' well completion reports that were filed with the NYSDEC for neighboring residential wells, core logs provided by Hanson, water levels measurements made at the site wells, site visits, and an inspection of rock core to specifically identify potential water-bearing fractures.

Drilling of the 2009 and 2010 series of wells provided information as to water occurrence in the bedrock. The only potential fractures or water producing zones noted by the driller were in the Onondaga Fm at wells 09-002, 09-003, 10-001 and 10-002 (Appendix C). No water was noted at the Onondaga/Akron contact at 09-001 and 09-002 (the other wells were not deep enough to reach the Akron Fm). The Onondaga/Akron contact is known to yield water to residential wells in the area. The well completion report for residential well LV874 (Kloesz) on Dalton Rd, which is adjacent to the quarry's east side, has a note by the driller that "most of the water comes in at 140'," which is also the depth given on the log as the Onondaga/Bertie (Akron) contact.

Alpha logged evidence of potential water bearing fractures in the rock core from four of the expansion area cores (Appendix B). These fractures exhibited mineralization or staining on the fracture surface, or they did not appear to represent fresh core breaks (caused by drilling). Some

of the potential water-bearing fractures were filled with silt, which may have occurred during the drilling process or may be indicative of prior deposition by water moving through the fractures.

Potential water-bearing fractures logged by Alpha in four of the rock cores from the expansion area are portrayed graphically on Figure 5. Potential fractures and water shows encountered during the drilling of the bedrock monitoring wells (Appendix C) also are shown on Figure 5. Some of the core logs provided by Hanson for the deep drill holes also had relevant information pertaining to ground water. Zones where circulation water was lost during the coring process were noted on the logs for the deep drill holes drilled in 1998. In rotary drilling, water is circulated down the drill string, out the drill bit, and up the annular space between the borehole wall and the drilling rods to remove the rock cuttings from the hole. Lost circulation zones are noted when the circulated water no longer returns the cuttings to the surface and are indicative of open fractures capable of moving ground water. The depths of the lost circulation zones were transferred to Figure 5. Figure 5 indicates that the vast majority of the features indicative of water movement, and potential water movement, are found within the Onondaga.

Most of the residential wells in the area penetrate both the Onondaga Fm and Bertie Group, based on their total depth (Appendix A) and the top of Bertie (Akron) elevation contours (Figure 4). Many nearby residential wells, that originally were open only in the Onondaga Fm, have been deepened or replaced with deeper wells during the last ten years (Table 1). There is a network of fractures within the upper 45 ft of the Onondaga that initially supplied enough water for residential use in the area. This fracture zone is the source of cascading water heard in wells 09-002, 09-003, 10-002 and the Campier well (Plate 1). The water within the upper fracture zone is draining downward toward the lower fracture zone at the Onondaga/Bertie contact. Wells that only tap the upper fracture zone in the area have commonly run low on water during droughty periods. The deeper wells can take advantage of deeper water-bearing fractures in the Onondaga and the fractured zone at the Onondaga/Bertie contact. There is no evidence of significant water shows below the contact. It is likely that the portion of the wells open in the Akron Fm, below

the contact with the Onondaga, act as sumps for additional storage when needed during droughty conditions.

3.2.2.1 Water Level Data

Water level data collected by Hanson since 2009 are included as Plate 1. The locations of the wells are shown on Figure 2, along with selected residential wells in the vicinity of the quarry. Hydrographs of the water level data from the expansion area wells are provided on Figure 6. Quarry wells 18 and 20 were included in the hydrographs because they are the closest quarry wells to the expansion area. The Campier well is included because it is the closest residential well to the expansion area that also has water level data. The Campier well and Well 20 (Crusher Run Plant Well) were being used as water sources throughout the monitoring period. The remaining wells were unused.

The lowest ground water elevations subsequent to the installation of the 2010 wells occurred around August 23, 2010 (Plate 1; Figure 6). The highest ground water elevations occurred during March 2011. The amplitude of the water level fluctuation during the nearly two-year monitoring period ranged from 21.24 ft at Well 18 (Garage Well) to 52.9 ft at well 09-002. In general, water levels in the expansion area wells began to rise in December, 2010, continued to rise through sometime in March, and then gradually fell through the summer.

Wells 20, 09-002, and the Campier well each experienced a relatively sudden, apparent drop in water level during early April 2011 (Figure 6). It was reported by the homeowner at the time of the water level reading on April 8 that the washing machine in the house had been operating all morning; consequently, the water level reading that day was likely much lower than it may have otherwise been. Also, well 09-002, 09-003 and the Campier well are known to have seasonal, or occasional, cascading water that can make it extremely difficult to obtain an accurate depth to water measurement (Plate 1). The cascading from the upper fracture zone at approximately 24 ft (Figure 5) may have ceased or diminished as the upper zone drained in early April; consequently, this could have allowed for a more accurate (lower) reading of the water level in certain wells. This may have caused the apparent large drop in water level elevation in wells 09-002 and the

Campier well that occurred around the first week of April, 2011. Well 20 also exhibited the same pattern as 09-002 and the Campier well at that time; however, cascading has not been noted in this well. A shroud has been used on the water level probe when measuring water levels in cascading wells since early April 2011 to protect the probe from cascading water and improve accuracy.

3.2.2.2 Water Table Configuration

A ground water elevation contour map constructed from the seasonal low ground water elevations (Figure 7). It is during the natural, seasonal low water level conditions when nearby residential wells potentially would be most vulnerable to water level decline due to quarry expansion and dewatering. The map shows the elevation of the water table surface as measured in the wells on August 23, 2010. Ground water flows from the areas of high water elevations toward low water level elevations perpendicular to the ground water elevation contours. The regional flow is to the north, but the local flow pattern is radially outward from recharge areas and inward toward discharge areas such as the quarry sump where the water is pumped out on a year-round basis.

A local ground water divide trends northeast to southward through the expansion area. Ground water flows away from the divide and toward discharge areas represented by streams, wetlands, springs, wells and the quarry. The interpretation of this local divide is based on the fact that the water level in well 09-003 is consistently higher than at the Campier well, which is located approximately 475 ft to the west of well 09-003 (Figure 6 and Plate 1). The interpretation of the presence of this local divide is also based on an estimate of the August 23, 2010 water level elevation at the residential well located at 1919 Honeoye Falls No. 6 Rd (formerly Rosenbloom). The estimate was made based on data from the Monroe County Department of Health (DOH) and from the historical water levels measured by Hanson at the quarry. The Monroe County and Livingston County DOHs measured water levels at residential wells in the vicinity of the mine from 2000 to 2005. The Rosenbloom well was part of that monitoring program from August 7, 2002 through February 6, 2004. The lowest water level elevation at the Rosenbloom well during that time frame was 595.2 ft amsl and was recorded on November 8, 2002. This water level

elevation is based on the measured depth to water of 101.8 ft and an assumed surface elevation of 697 ft amsl (from the topographic map). The water level elevation recorded on November 11, 2002 at quarry well 18 (garage well), which was not in use, was 606.68 ft amsl (11.48 ft above the water level at the Rosenbloom well). The August 23, 2010 water level elevation at well 18 was 605.26 ft amsl; consequently, the estimated water level at the Rosenbloom well for that date is 593.78 ft amsl (11.48 ft below the water level at well 18).

3.3 Future Conditions of Water Table at end of Mining

Hydrogeologic cross sections A-A', B-B' and C-C' were constructed and are included as Figures 9, 10 and 11. The existing topography, top of rock surface and top of Bertie (Akron) surface are depicted on the cross sections. The seasonal low water table, represented by the August 23, 2010 ground water contours (Figure 7), is shown on each of the cross sections. Hanson's mine reclamation plan for the Honeoye Falls quarry, including the existing quarry and the expansion area, is included as Figure 11. Figure 11 shows the proposed quarry floor topography and the locations of the quarry faces and benches. The proposed quarry floor elevations were transferred to the hydrogeologic cross sections. The cross sections depict how the mine plan is to excavate the Onondaga Fm limestone down to, or almost down to, the Akron Fm. The mine plan was constructed by Hanson personnel and the top of the Bertie Group (Akron) elevation was interpreted by Alpha; consequently, there are subtle differences in the proposed quarry floor and the top of the Akron Fm surface as shown on the cross sections. It is Alpha's understanding that Hanson has no intention to mine below the Onondaga Fm.

The maximum water table gradients, sustained under existing conditions in the vicinity of the expansion area (Figure 7), were used as a guide to predict the drawdown gradients and extent of water table drawdown impacts outward from the seepage face on the quarry walls. No seepage face is predicted on cross section C-C' (Figure 10) for the northern quarry wall or on cross section A-A' (Figure 8) for the northern half of the western quarry wall (generally north of the wetland) during the seasonal low conditions. No seepage face is predicted in these areas during seasonal low water table conditions because the elevation of the seasonal low water table during existing conditions is already at, or below, the proposed quarry floor in those areas. The presence

of the quarry cannot lower the water table elevation when the water table is below the quarry floor; consequently, no changes to the water table are predicted for those areas during the dry season.

Residential wells north of the expansion area, along Honeoye Falls Rd. No. 6, will not be impacted during seasonal low water table conditions when the potential for impact to residential wells due to quarry expansion is the greatest. Likewise, residential wells located west of the northern portion of the expansion area, such as the Campier well and wells to the west of Oak Openings Road, will experience no impact from the quarry expansion during seasonal low water table conditions. The reason these residential wells will not be impacted is because the dry season water level elevation in these wells under existing conditions is already below the base of the proposed quarry floor.

Cross section B-B' and C-C' indicate that seepage faces are predicted for the southern portion of the proposed western quarry wall and on the proposed southern wall during seasonal low water table conditions. The seepage faces are anticipated to be approximately one-third the vertical distance between the mine floor (base of Onondaga Fm aquifer) and the elevation of the existing seasonal low water table. The impacts from water table (bedrock aquifer) drawdown west of the southern portion of the proposed mine expansion area are projected to extend approximately 625 ft westward from the quarry face when the water table is at its seasonal low (Figure 9). The projected impacts in that area are all within the Hanson property boundary and there are no residential wells within that area. The drawdown impacts south of the proposed southern quarry face are anticipated to extend approximately 500 ft south of the mine (Figure 10). The projected drawdown impacts south of the proposed expansion area also are still within the Hanson property only, and no residential wells are present in that area. The ground water divide that currently exists within the proposed expansion area during low water conditions will remain relatively unchanged because the water table will be at, or below, the quarry floor. The location of the divide will shift westward in the area west of the southern half of the proposed expansion area by less than 100 ft (Figure 9).

Seepage faces will exist along the northern, western and southern quarry walls during times when the water table is higher. There will be no quarry wall on the eastern side of the expansion area; the eastern side will be open to the rest of the existing, permitted mine all the way to the existing eastern quarry face (Figure 11). Seepage into the proposed expansion area will flow southward across the quarry floor to the southern wall, then flow eastward toward the sump at its current location (see Section 3.5). There is no reason to expect any changes in water quality in any of the residential wells since ground water flow from all directions is toward the mine.

3.4 Future Conditions of Wetland and Shallow Perched Ground Water

The proposed expansion area does not include any portion of the wetland. The excavation of the bedrock in the expansion area will have no impact on the presence of the wetland because the bedrock aquifer in the expansion area does not discharge to the wetland. The removal of the overburden in the expansion area will remove a relatively small portion of the recharge area for the wetland. The wetland is currently recharged via direct precipitation; influx of ditches and streams from the south; runoff from north, south and east; and from the perched ground water flow in the unconsolidated deposits above bedrock. The portion of recharge area that will be removed is approximately 31 acres as defined topographically. Areas outside the proposed expansion area perimeter berm that currently contribute runoff and shallow, perched ground water flow to the wetland will continue to do so at full build out of the expansion area. The removal of 31 acres of drainage area from the outlet stream is equivalent to removal of less than 2% of the 1,820-acre drainage basin for that stream (Figure 12). The stream that drains the wetland has been documented as ephemeral and goes dry sometime in June. The stream is anticipated to remain ephemeral after the proposed expansion area has reached full build out.

3.5 Adequacy of Present Sump to Serve Expansion Area

The existing sump should be able to serve the mine through full build out as it is shown on the existing mine reclamation plan (Figure 11). The existing mine reclamation plan indicates a quarry floor that extends below an elevation of 570 ft in the southwest corner of the mine at full build-out. Seepage from the quarry walls of the expansion area and direct precipitation will flow southward and southeastward across the floor of the quarry until it reaches the southwestern

corner of the quarry. The water will then pond against the southwestern wall until the elevation of the ponded water rises to approximately 576 ft amsl. The ponded water can then flow by gravity across the mine floor, eastward to the sump. This scenario assumes that the underlying Akron Fm is insufficiently fractured to convey water to the sump through the bedrock. A pump could be employed to transfer water from the ponded area to the sump if that area needed to be kept dry during quarrying operations. Alternatively, if the mine floor in the southwest corner was kept above 575 ft amsl, there would be no ponding. It would be necessary to continue maintaining the water level in the sump between approximately 565 ft and 570 ft amsl in order to maintain a dry floor throughout the quarry.

4.0 CONCLUSIONS

The hydrogeologic analysis of the proposed expansion of the Honeoye Falls quarry was conducted for Hanson Aggregates New York LLC. A detailed hydrogeologic evaluation was conducted principally by reviewing existing information from literature, Hanson's records, NYSDEC logs, and publically available water level data; conducting inspections of the site; rock core and drill cuttings; installing a wetland piezometer; and analyzing water level and related hydrogeologic data. The objectives of the investigation were to provide information about the physical characteristics of the ground water system within and around the expansion area, describe the anticipated changes that will occur to that system when the mine is at its maximum extent, evaluate the potential impacts to neighboring residential wells and an adjacent wetland, and evaluate the adequacy of the existing sump to serve the mine as expansion progresses. The following are the primary conclusions derived from the investigation:

• The site hydrology is comprised of a localized, shallow, perched ground water system and a water table aquifer. The perched system is primarily comprised of the wetland southwest of, and adjacent to, the expansion area. The water table aquifer occurs within the fractured limestone bedrock of the Onondaga Fm and extends down into the contact with the underlying Akron Fm of the Bertie Group.

- Regional ground water flow is northward, while local ground water flow is influenced by local ground water recharge and discharge areas. Ground water in the vicinity of the existing quarry flows toward the quarry from all directions.
- A local ground water divide exists within the expansion area. Water east of this divide flows toward the quarry, while water on the opposite side of the divide flows toward the north and west.
- Most of the residential wells in the vicinity of the active mine and the expansion area extend through the Onondaga Fm and into the underlying Bertie Group over a hundred feet below the surface.
- Water level data collected at the site wells and nearby residential wells since 2009 indicate that the seasonal low water table conditions, subsequent to installation of the 2010 monitoring wells, occurred on or about August 23, 2010. The water table generally rises from December through March, then falls throughout the summer.
- Quarry expansion and pump out will have the greatest potential for impacting nearby residential wells during seasonal low water table conditions.
- The seasonal low water table is already at or below the future quarry floor in the northern half of the expansion area; consequently, there will be no further drawdown of the water table beyond what normally occurs during the dry season.
- Residential wells along Honeoye Falls No. 6 Rd north and west of the quarry entrance will not be impacted during seasonal low water table conditions when the potential for impact is the greatest; likewise, the Campier well directly west of the expansion area will not be impacted at that time. These residences are all on the opposite side of the ground water divide that runs through the expansion area.
- Seepage faces are predicted for the quarry walls on the southern portion of the expansion area during the seasonal low water table conditions; consequently, there will be some drawdown of the water table south and southwest of the mine during that time. The drawdown impacts in these areas extend outward from the mine less than 700 feet and occur only within Hanson property, where there are no residential wells.
- The wetland to the southwest of the proposed expansion area will experience negligible impact from excavation of the expansion area. The wetland is perched above bedrock and does not receive recharge from the water table aquifer (bedrock) in the expansion area.

The removal of the unconsolidated material within the expansion area will remove approximately 2% of the drainage system that contributes to the stream flow at the wetland outlet. The stream presently is ephemeral and will remain so after quarry expansion.

• The present sump location can continue to serve the quarry throughout the excavation of the expansion area. Seepage and precipitation will flow southward across the quarry floor, form a small pond against the southern wall of the mine until an elevation of approximately 575 ft amsl is reached, after which the water will begin to drain eastward toward the present sump.

REFERENCES

- Muller, E.H., and D.H. Cadwell, 1986; Surficial Geologic Map of New York Finger Lakes Sheet; New York State Museum – Geological Survey.
- Natural Resources Conservation Service, Web Soil Surveys for Livingston and Monroe Counties, National Cooperative Soil Survey.
- Spectra Environmental Group, Inc., 2000, Sump Deepening Impact Assessment March 9-17, 2000, Pump Test & Long Term Monitoring Report; Unpublished Consulting Report for Hanson Aggregates East, 162 p.

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TABLE

TABLE 1 Deepened or Replaced Wells in the Vicinity of Honeoye Falls Quarry Hanson Aggregates New York, LLC Alpha Project No. 11110

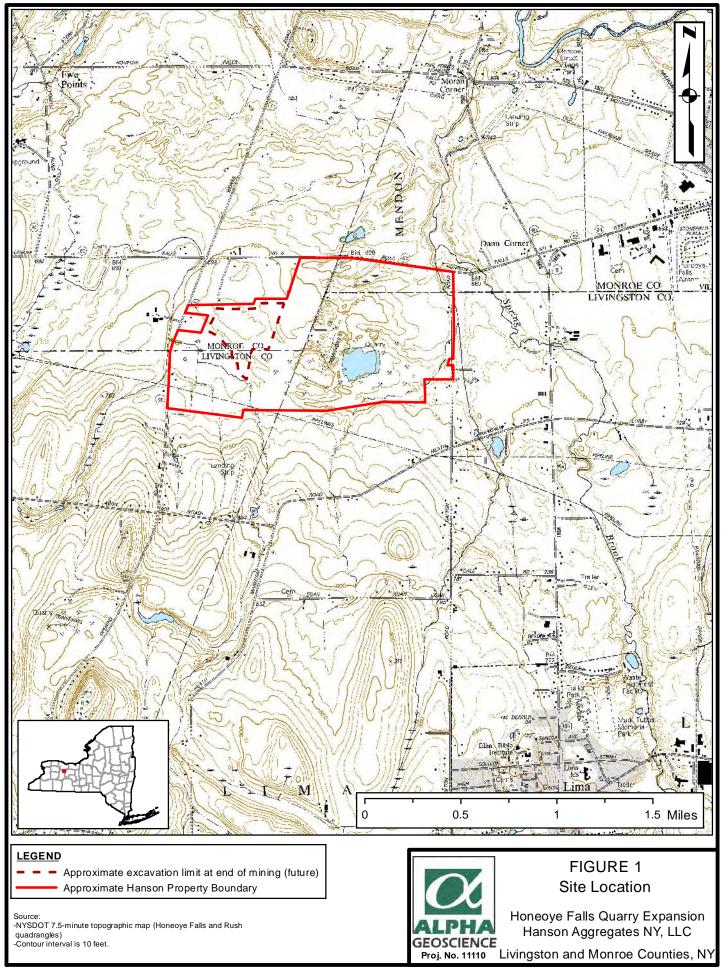
	NYSDEC WELL ID	Last Known Resident at Address	Action	Year	Elevation at Grade (approx)	Existing Well		Former Well		
Address						Total Depth	Bedrock at Well Base	Total Depth	Bedrock at Well Base	Notes
Dalton Rd, near county border	LV798	Koch	New Well	2002	661	150	Bertie			
1110 Dalton Rd		Clark	Replaced well	post-2004	678	113	Onondaga	54	Onondaga	
1149 Dalton Rd	LV743	Travers	Deepened well	2001	708	120	Onondaga	65	Onondaga	
1150 Dalton Rd	LV951	Farron	Replaced well	2005	678	150	Onon/Bertie Contact	61.5	Onondaga	
1168 Dalton Rd	LV874	Kloesz	Replaced well	2003	683	160	Bertie	67.85	Onondaga	Driller noted the Bertie/Onondaga contact was at 140 ft and that "most of the water comes in at 140 ft"
1600 Honeoye Falls No. 6 Rd.		Burnell	Deepened well	2009	684	155	Bertie	108	Onondaga (likely)	"encountered good volume of water at 135', continued to 155' to guarantee a good reservoir" - 10/19/2009 email from Tim Nothnagle (Nothnagle Drilling) to M. Lewis (Hanson)
1820 Honeoye Fall No. 6 Rd	M01741		Deepened well	2009	663	180	Bertie	127	Bertie	pond well - on Pluta property
1820 Honeoye Fall No. 6 Rd	M01742	Mrs. Pluta	Replaced well	2009	702.5	141	Bertie	120	Onondaga	"Broke up limestone" at 120 ft (Driller's Log)
1855 Honeoye Fall No. 6 Rd	M01756	Knab	Deepened well	2009	721.5	180	Bertie	140		Bedrock should be Bertie Fm - personal communication from R. Moravec (driller) to S. Trader (Alpha)
1919 Honeoye Falls No. 6 Rd		Rosenbloom	Deepened well	mid 1990s	697	120	Bertie	70	Onondaga	Info. from M. Lewis (Hanson) phone call with Ms. Rosenbloom on 8/18/2009; DOH records
525 Works Rd	M01740	W. Pluta	Deepened well	2009	674	119	Bertie	89	Onondaga	
625 Works Rd		Altamura	Deepened well	2009	690	130	Bertie	115	Onondaga	NYSDEC - personal communication to M. Lewis (Hanson) re: well info obtained by NYSDEC on 9/23/2009
916 Works Rd		Campier	Deepened well	post-2003	705	147	Bertie	119	Onondaga	

Intrpretation of bedrock at base of well based on top of Akron elevation contours on Figure 4, with additional information in Notes column

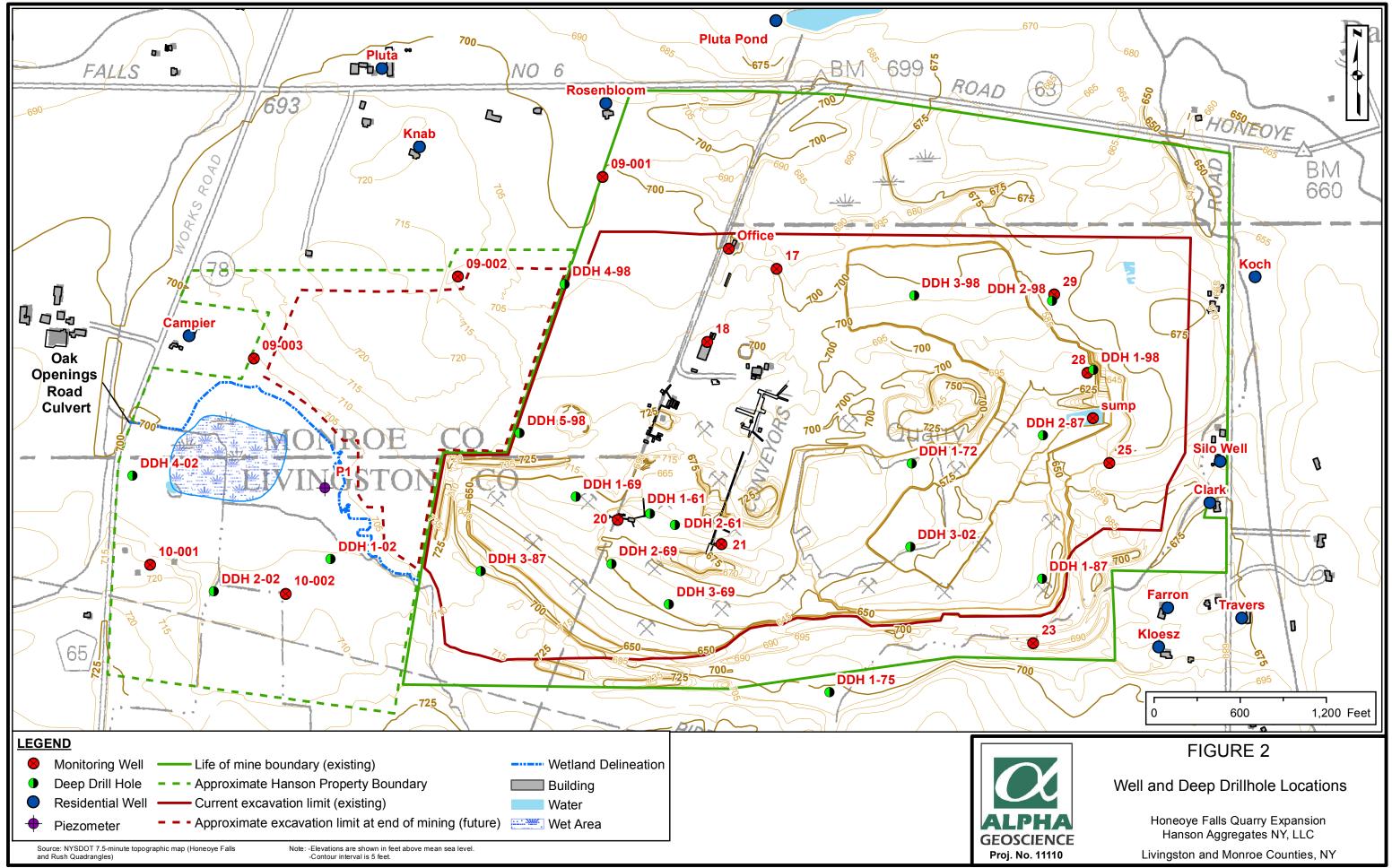
Grade elevations are from driller's log or estimates from topo map

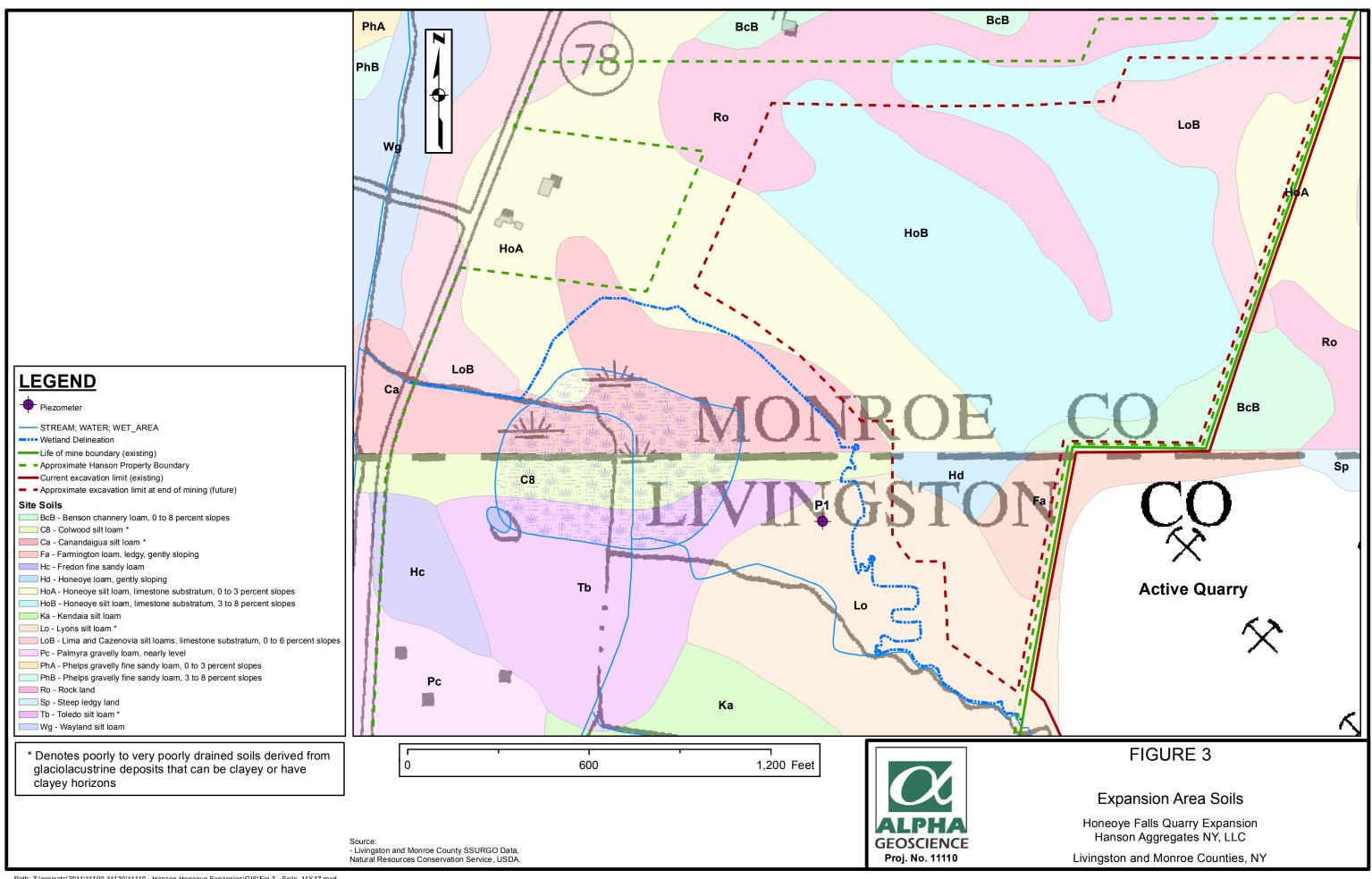
Sources of information include Monroe County Department of Health, Livingston County, NYSDEC Well completion Reports, and personel communication with residents and drillers

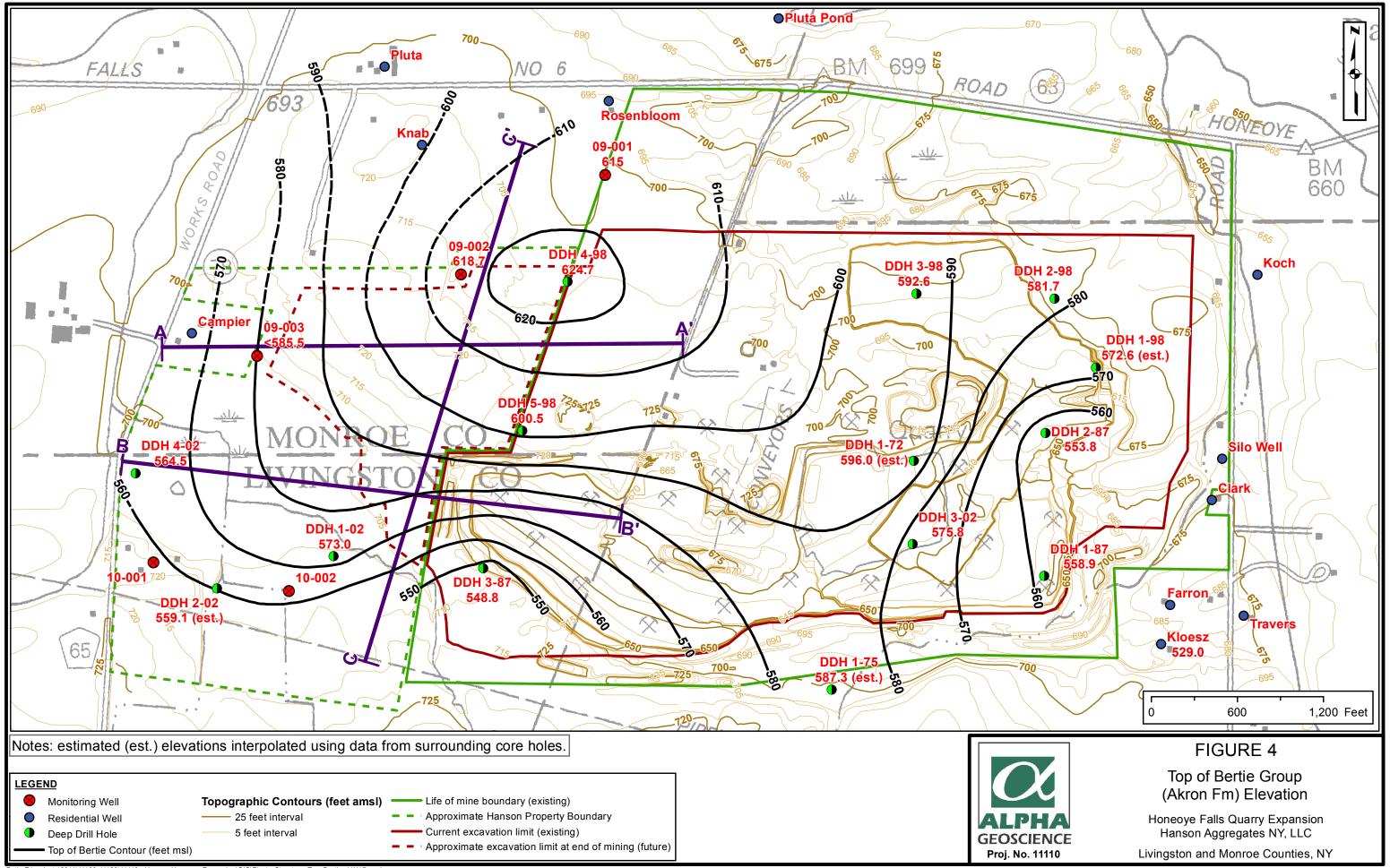
FIGURES



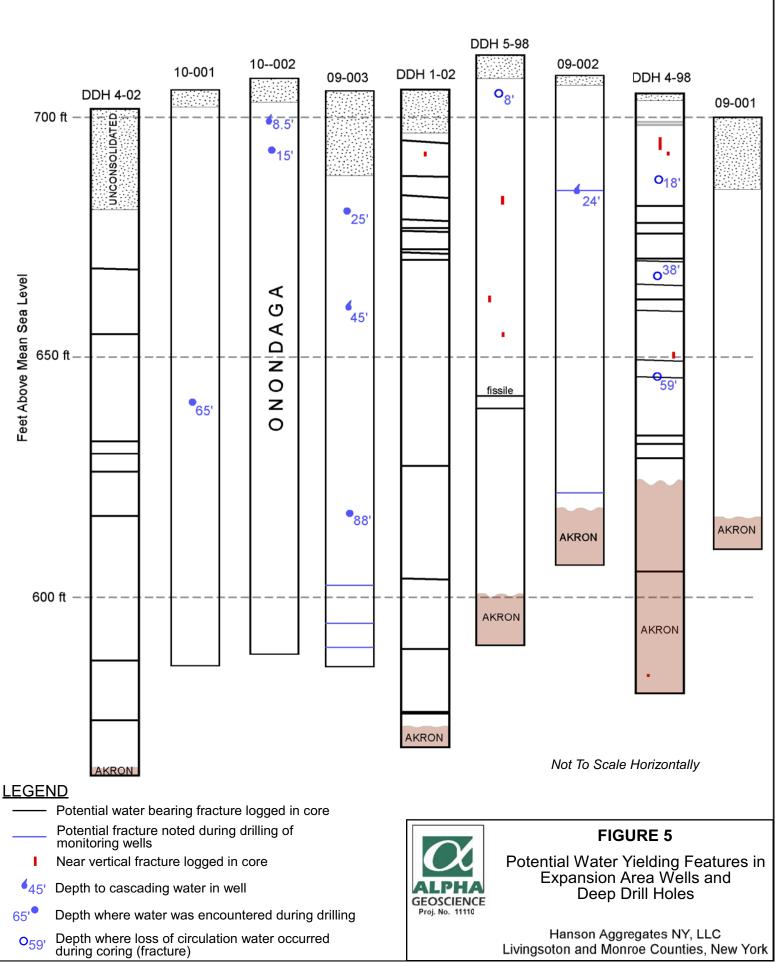
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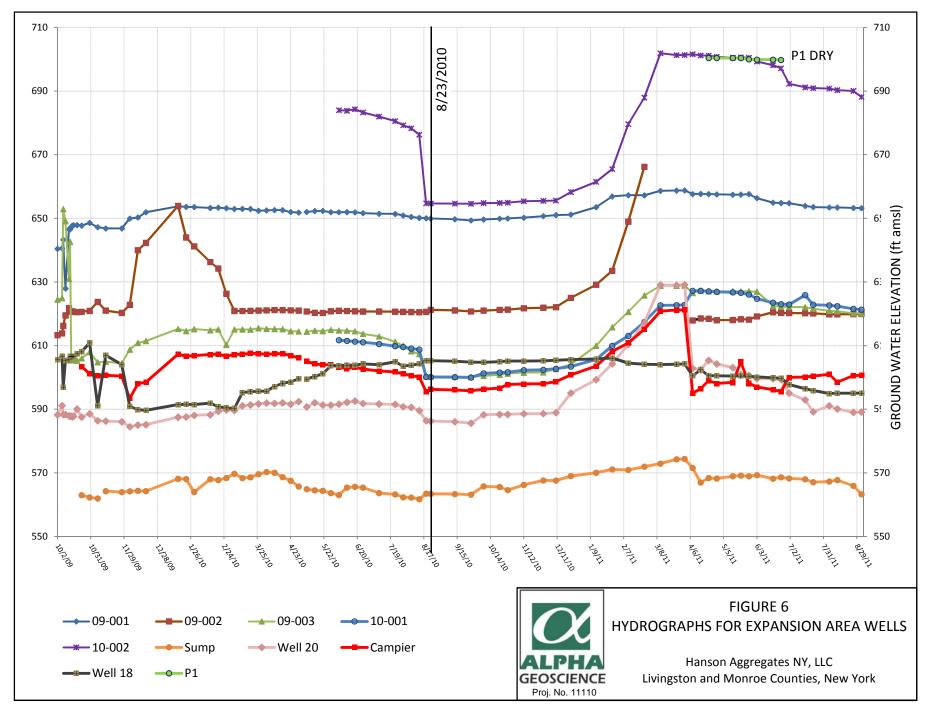




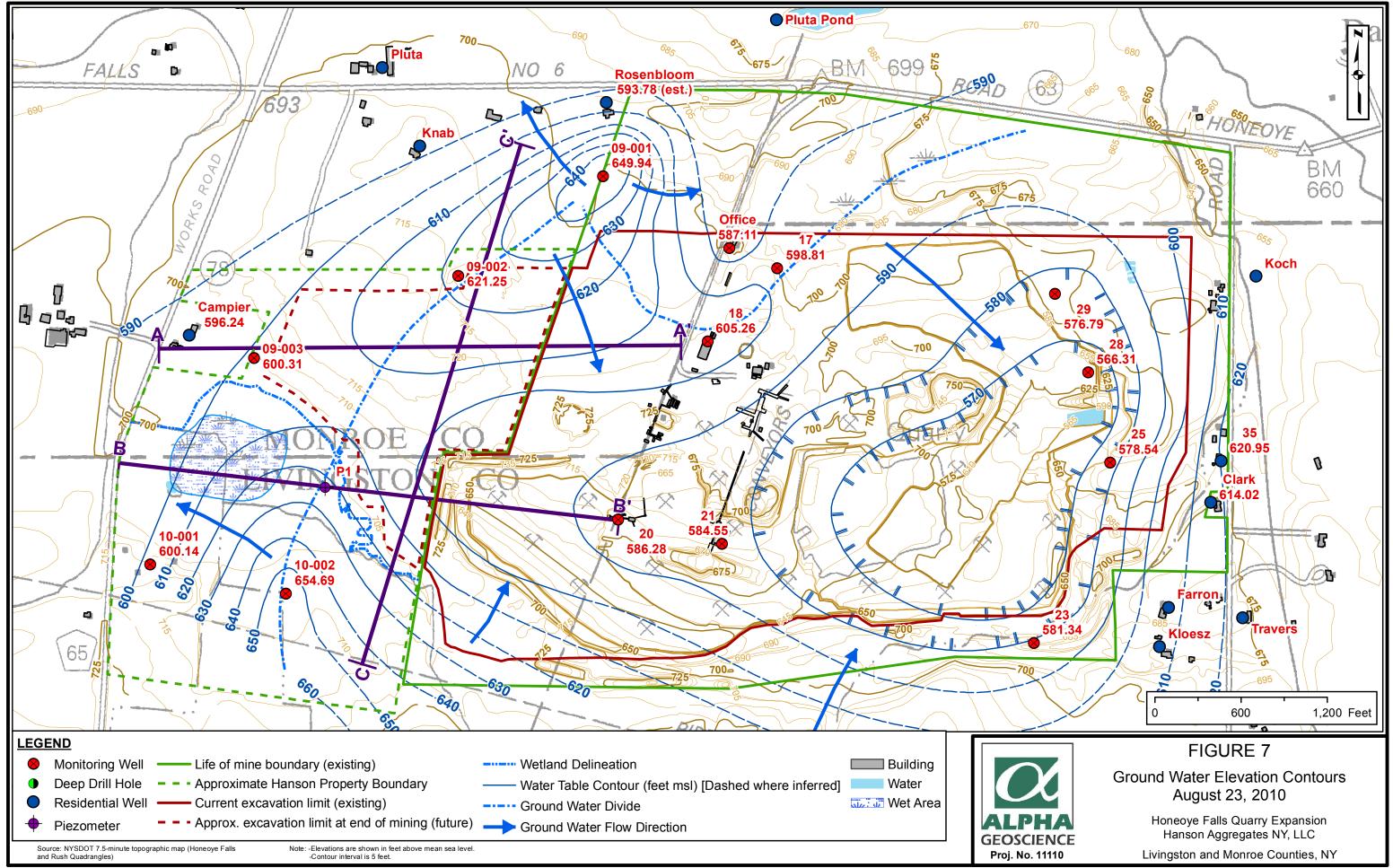
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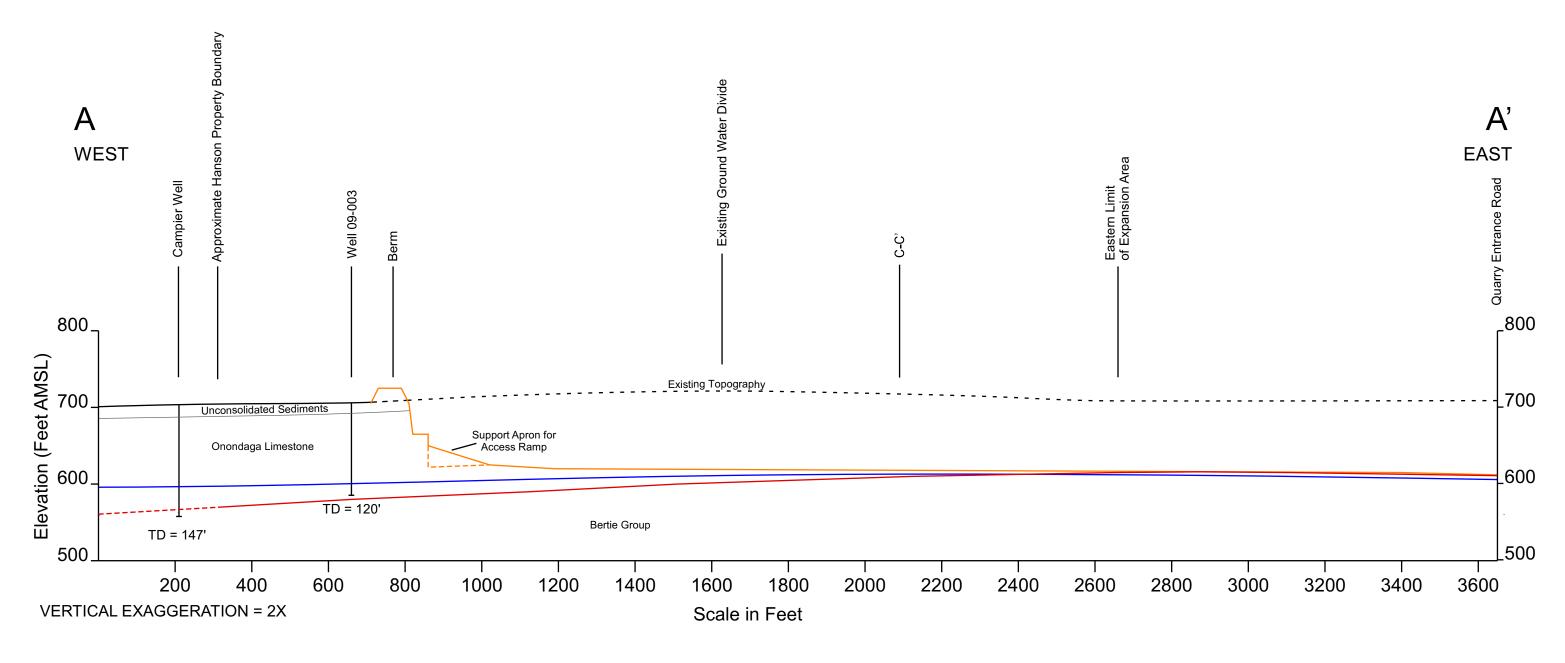
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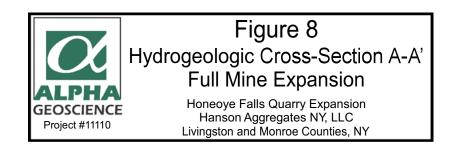


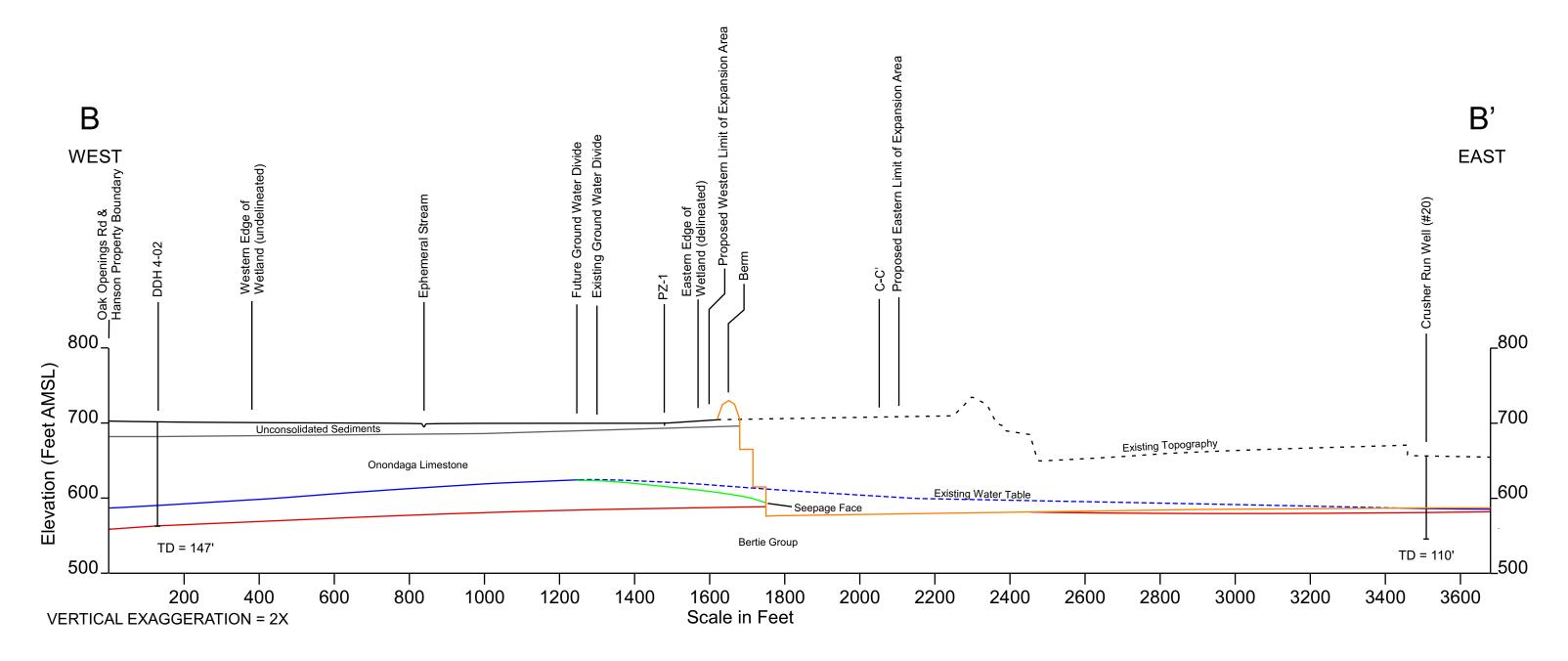
<u>LEGEND</u>

- —— Proposed Quarry Expansion
- —— Top of Bedrock Surface
- —— Existing and Future Water Table
- ----- Top of Bertie Group (Akron Fm)

NOTES:

Well locations shown are extrapolated to the cross-section line (refer to Figure 7) Water Table and Top of Akron surface are based on the contours in Figures 7 and 4, respectively. Quarry profile based on contours in Figure 12.



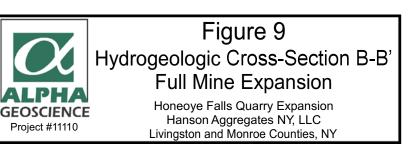


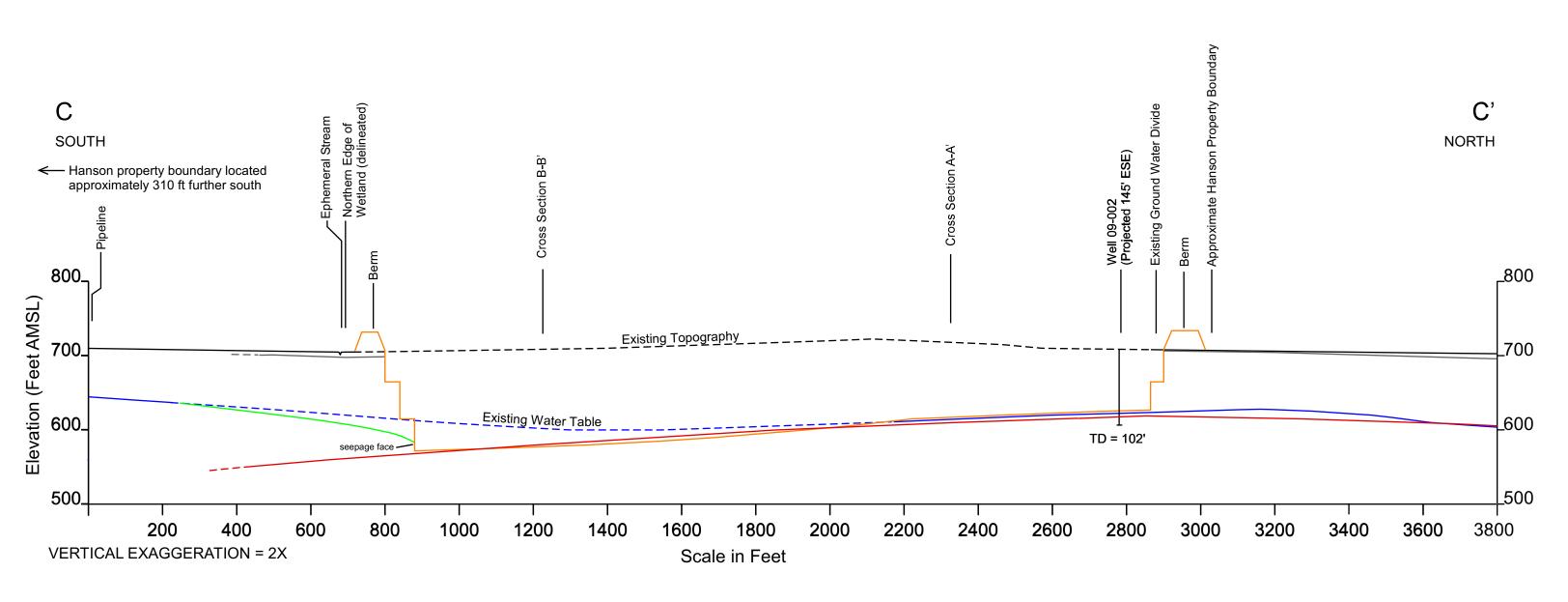
<u>LEGEND</u>

- ----- Proposed Quarry Expansion
- —— Top of Bedrock Surface
- —— Top of Bertie Group (Akron Fm)
- Water Table
- ----- Future Water Table at End of Mining

NOTES:

Well and deep drill hole locations locations shown are extrapolated to the cross-section line from Figures 7 & 4, respectively. Water Table and Top of Akron surfaces shown are based on the contours in Figures 7 and 4, respectively. Quarry profile based on contours in Figure 12.





LEGEND

NOTES:

Well location shown is extrapolated to the cross-section line (refer to Figure 7) Water Table and Top of Akron surfaces shown are based on the contours in Figures 7 and 4, respectively. Quarry profile based on contours in Figure 12.

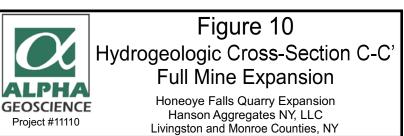
Proposed Quarry Expansion

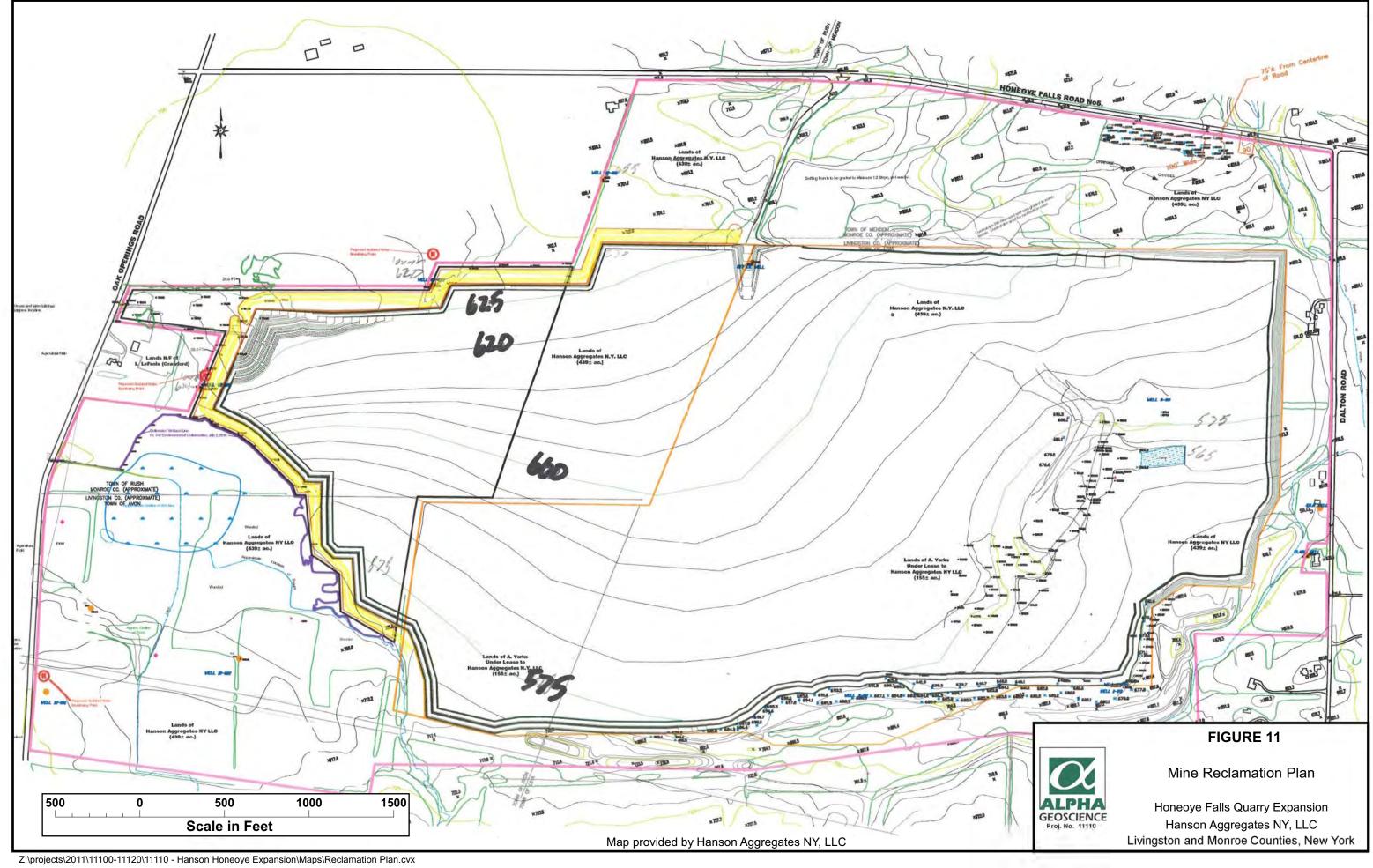
Top of Bertie Group (Akron Fm)

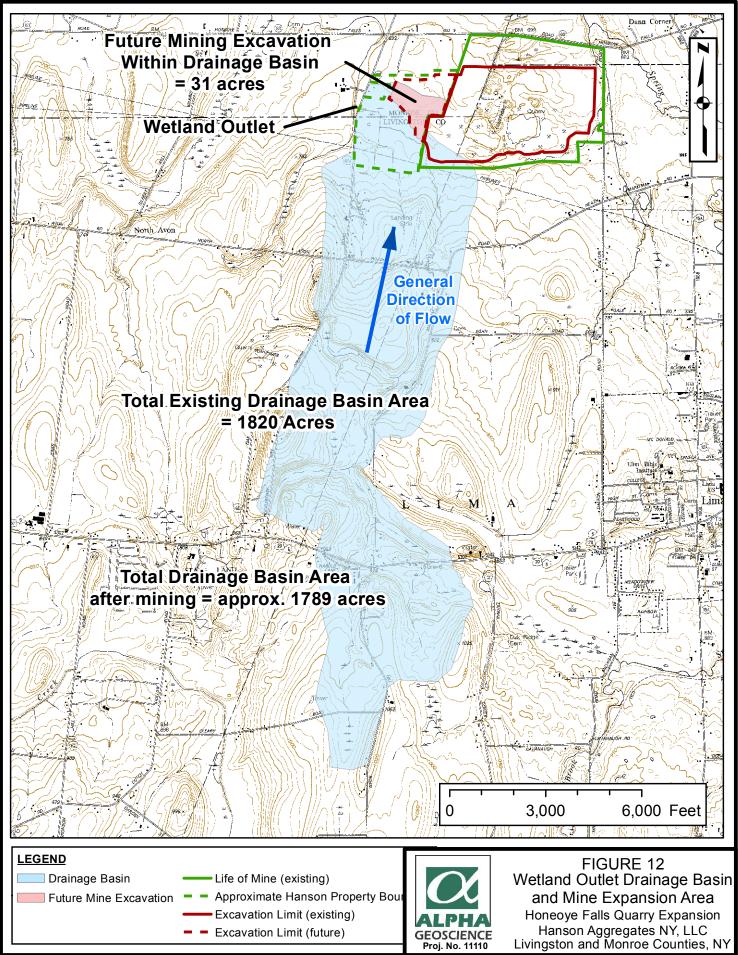
Future Water Table at End of Mining

Top of Bedrock Surface

Water Table







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PLATE

		n Well #18 (Qua ot Garage Well - i in use)	not Run P	0 (Crushe lant Well - for dust ression)		(water	Well #21 (Pr Crusher W used for d supressio	/ell - dust	Well #	23	Well #	#24	Well	#25	Well	l #28	Well	# 29	Well 0	9-001	Well 09-	002	Well 09-(₀₀₃ Ca	mpier Well (9 Works Rd)		Residence 110 Dalton Rd	Well #35 Rd. Sil		Well 10-0	01 \	Vell 10-002	Wetla Piezomet		ak Opening Culvert		Sump
leasuring Point Elev. (ft)	688.07	712.36		656.5	700.27	7	659.7		678.4	4	677.	.9	662	2.7	578	8.4	67	0.0	702	2.2	710.4		707.4		705.4		678.1	66	5.1	707.19		709.72	703.1	1	699.91		610.5
Well Depth (ft. below grade)	125	120		110	111		110		131		145	5	10	5	3	30	10	0.0	90.	.0	102.0		120.0		147.0		113.0	11	10	125		120	2.7				
DATE	Depth to Water Elevation	Water Lev	el Water	Water Level Elevatio	Water	Water Level levation	Water L	ever	eptn to Water	Water Level Elevation	Depth to Water	Water Level Elevation	Depth to Water	Water Level Elevation	Depth to Water	Water Level Elevation	Depth to Water	Water Level Elevation	Depth to Water	Water Level Elevation	Water	Water Level levation	Water		epth to Vater Elevatio	Water	Water Level Elevation	Depth to Water	Water Level Elevation	Water L	ever	th to ater Elevation	Water	Level	Vater		epth to Nater Eleva
9/2/2011 8/26/2011	93.57 594.5 93.11 594.9	6 117.31 <u>595</u> .	09 67.36 05 67.49	589.01	109.33 5 110.41 5	589.86	44.55 6	15.15 8	36.22 (35.57 (592.83	87.47 86.32	591.58	78.23 78.19	584.47 584.51	9.33 9.78	569.07 568.62	86.94 87.17	583.06 582.83	48.93 48.89	653.26	90.47 (90.52 (619.90	87.27 6 87.21 6	620.15 10	04.72 600.6 04.84 600.5	9 50.55 7 50.41	627.53 627.67	33.42 32.78	631.68 632.32	85.88 62 85.62 62	21.57 19	.56 688.16 .66 690.06	DRY DRY	1	DRY	4	17.21 563 14.56 565
8/12/2011 8/5/2011	92.46 <u>595.6</u> 92.41 <u>595.6</u>	6 117.4 <u>594</u> .	03 66.39 06 65.41 07 04	591.09	110.67 5 110.55 5	589.72	44.86 6	14.84 8	34.17	594.23	85.52 85.41	592.49	78.14	584.56 585.49	9.41 8.79	568.99 569.61	86.79	583.21	48.74 48.72	653.43	90.59 (90.57 (619.85	86.55 6 86.41 6	620.95 10	06.91 598.5 04.41 601.0	0 49.47 0 48.98	628.61 629.10	• · · · ·	632.88 633.33	84.79 62 84.54 62 04.05 62	22.65 18	.41 <u>690.31</u> .91 <u>690.81</u>	DRY DRY			43	12.77 <u>56</u> 13.21 <u>56</u>
7/22/2011 7/15/2011 7/1/2011	92.34 595.7 89.67 598.4 88.43 599.6	0 115.91 596.	3967.314563.557861.44	592.95	109.22 5 107.21 5 104.77 5	593.06	44.13 6' 43.71 6' 42.37 6'	15.99 8	33.77 32.56 30.44	595.84	84.13 83.54 82.67		77.32 76.94 76.91	585.38 585.76	9.33 9.77 9.51	569.07 568.63	86.57 86.21 85.82	583.43 583.79 584.18	48.61 48.24 47.39	653.91	90.28 (90.24 (90.17 (620.18	85.77 6 85.24 6 85.22 6	622.12 10	04.98 600.4 05.27 600.1 05.41 600.0	3 48.67 4 48.51 0 48.44	629.41 629.57	30.55 30.14 28.21	634.55 634.96	84.35 62 81.31 62 84.27 62	25.88 18	.77690.95.52691.20.41692.31	DRY DRY DRY		DRY DRY DRY	42	13.41 56 12.51 56 12.23 56
6/24/2011 6/17/2011	87.24 600.8 86.95 601.1	3 112.61 <u>599</u> .	75 57.11 39 56.91	599.39	104.77 5 101.51 5 100.41 5	598.76	42.37 6 39.41 62 38.98 62	20.29 7	79.13	599.27	81.54 80.81	595.25 596.36 597.09	76.91 76.17 75.21	586.53 587.49	9.31 9.21 8.44	569.19 569.96	85.77 85.29	584.23 584.71	47.33 47.21	654.82	90.17 (90.14 (89.92 (620.28	85.17 6 84.85 6	622.19 10	09.88 595.5 09.27 596.1	40.44 3 46.74 4 46.21	631.34 631.87	27.43	637.67 638.89	84.16 62 83.71 62	23.03 12	.55 697.17 .56 698.16	3.34 3.24	699.77 I	DRY 0.17 69	4	1.88 56 12.33 56
6/3/2011 5/27/2011	86.74 601.3	3 112.21 600. 0 111.96 600.	15 56.88 40 55.91	599.62	99.94 6	600.33	38.71 62 38.44 62	20.99 7	78.22	600.18	79.87 79.54		74.93	587.77 587.99	8.41 8.34	569.99 570.06	85.27 84.66	584.73 585.34	45.79 44.54	656.36	91.23 (92.24 (619.19	80.41 6 80.27 6	626.95 10	08.41 597.0 07.27 598.1	4 40.21 0 44.67 4 43.54	633.41 634.54	25.53 24.61	639.57 640.49	82.45 62 81.13 62	24.74 10	.41 <u>699.31</u> 23 700.49	3.23	699.88	0.25 69 0.50 69	97.08 4	1.21 56 1.54 56
5/20/2011 5/13/2011	86.47 601.6 86.61 601.4	0 111.9 600.	46 55.66 45 53.41	600.84	98.41 6 97.91 6	601.86		_	77.74	600.66	79.22 79.54	598.68 598.36	74.11 73.92	588.59 588.78	7.88	570.52 570.49	84.51 84.8	585.49 585.20	44.68 44.71	657.47	92.11 (92.37 (618.31	80.31 6 80.26 6	627.05 10	00.54 604.8 06.97 598.4	7 42.77 4 41.77	635.31 636.31	24.55 24.54	640.55 640.56	80.57 62 80.44 62	2 <mark>6.62</mark> 9.	11 700.61 22 700.50	2.71	700.40	0.50 69 0.50 69	97.33 4	1.33 56 1.54 56
4/29/2011 4/22/2011	86.57 601.5	0 111.84 600. 3 111.79 600.	52 52.26 57 51.11		97.91 6 97.51 6		37.51 62 37.33 62	_	77.92	600.48	79.22 79.41	598.68	73.77 73.81	588.93 588.89	8.72 5.86	569.68 572.54	83.56 83.97	586.44 586.03	44.62 44.51	657.53	92.41 (91.97 (618.01	80.31 6 80.27 6	627.05 10	07.32 598.0 06.41 599.0	9 42.93 0 41.59	635.15 636.49	24.22 24.17	640.88 640.93	80.27 62	26.92 8.	91 700.81 57 701.15		700.38	0.38 69 0.50 69	97.20 42	12.27 56 12.11 56
4/15/2011 4/8/2011	86.21601.886.26601.8	6 109.96 602.	40 54.11 52 53.61			602.81 602.01	37.49 62 37.51 62	22.21 7	78.91 78.93	599.49 599.47	80.57 80.62	597.33	74.51 74.54	588.19 588.16	5.11 4.65	573.29 573.75	83.23 83.31	586.77 586.69	44.47 44.52	657.63	91.88 (92.50 (618.54 617.92	80.11 6 80.80 6	627.25 10	08.97596.410.41595.0	4 40.97 0 41.05	637.11 637.03	24.11 24.15	640.99 640.95	79.94 62 79.97 62	27.25 8.	52 701.20 11 701.61	Installed 04	1/20/11	0.42 69	97.24 4	I3.51 56 38.95 57
4/1/2011 3/25/2011	82.77 605.3 82.94 605.1		2527.331527.54	628.96	95.13 6 95.23 6	605.04	31.446231.5462	28.16	70.44 (70.88 (607.52	77.37 77.41	600.53 600.49	72.68 72.88	590.02 589.82	2.24 2.11	576.16 576.29	76.31 76.37	593.69 593.63	43.37 43.41	658.74		eadings	78.51 6 78.57 6	628.79 8	4.17621.24.21621.2	4 37.51 0 37.57	640.57 640.51	20.33 20.44	644.77 644.66	84.41 62 84.48 62	22.71 8.	37701.3541701.31				3	36.11 57 36.23 57
3/11/2011 2/25/2011	82.91 605.1 84.21 603.8	6 108.22 <u>604</u> .	05 27.41 14 39.26	617.24	96.44 6	605.10 603.83	35.33 62	24.37 7	-	602.99	77.82 78.27	599.63	72.93 75.27	589.77 587.43		575.99 573.67	76.43 77.23	593.57 592.77	43.51 44.91		44.21 (666.21	78.54 6 81.58 6	325.78 9	4.57 620.8 00.23 615.1	4 37.61 8 44.13		20.72 25.11	644.38 639.99		17.42 21	81 701.91 .77 687.95				3	37.58 57 38.54 57
2/11/2011 1/28/2011	86.11 601.9)9 52.22	604.28	108.41 5	591.86	55.79 <mark>6</mark> 0	03.91 8	34.51	593.89	89.72	588.18	80.44	583.79 582.26	7.41	572.44 570.99	81.17	588.83	45.27	656.88	76.91 (633.51	91.58 6	615.78 9	7.23 <u>608.1</u>	8 51.17	626.91	35.19	629.91	97.27 <mark>6</mark> (9.92 44	.11 679.61 .23 665.49				3	39.57 57 39.41 57
1/14/2011 12/23/2010	89.11 598.9		59 61.44		110.44 5	590.70 589.83	69.77 5 8	89.93	91.11	585.18	94.14	584.24 583.76	83.14	580.25 579.56		570.49 567.52		578.23		653.52 651.18	85.41 (625.01	97.41 6 103.27 6	604.09 10	01.85 603.5 04.61 600.8	6 59.23 0 61.47	616.61	42.77	622.33		03.42 51	.22 661.50 .44 658.28				4	10.44 5 11.50 50
12/10/2010 11/29/2010	89.36 598.7	6 106.97 605. 1 107.14 605. 6 107.19 605.		588.62	112.55 5		74.55 58	85.15 9	95.92 96.11	582.29		581.96				565.98	92.39 92.44	577.56	51.12 51.44	650.71	88.33 (88.51 (88.67 (621.91	104.73 6 105.77 6 105.84 6	601.59 10	06.77598.607.39598.007.44597.9	4 63.24 2 63.50	614.58	43.22	621.88	104.47 60 104.81 60 104.91 60	02.38 54	.13655.59.21655.51.33655.39				4	12.92 50 12.88 50 14.26 50
11/12/2010 10/29/2010 10/22/2010	89.86 598.2	6 107.19 605. 1 107.21 605. 6 107.43 604.	17 67.91 15 68.10 93 68.11	588.40	112.67 5	587.68 587.60	74.97 58	84.73 9	96.21 96.57	581.83	96.17		84.27	578.54 578.43	12.11	566.49 566.29	92.88 93.13 93.27	576.87	51.96 52.19		89.11 (521.31	106.17 6	601.19 10	07.44 597.9 07.67 597.7 08.77 596.6	7 63.71 4 63.85 4 64.13	614.23	43.67	621.43	104.91 60 105.55 60 105.67 60	01.64 54	.33 655.39 .77 654.95 .86 654.86				4	14.26 5 15.91 5 14.01 5
10/22/2010 10/8/2010 9/27/2010	90.21 597.8	6 107.43 604. 6 107.59 604. 0 107.55 604.	68.21	588.29	112.88 5	587.46 587.39 586.67	75.22 58	84.48	96.85 96.87 97.22	581.53		581.49 581.09		578.19	12.36 12.41	565.99	93.41 93.88	576.59	52.24 52.51 52.80		89.41 (621.01	106.88 6 107.20 6	600.48 10	09.11 596.0 09.11 596.3 09.60 595.8	4 64.13 0 64.41 1 64.21	613.67	44.11		105.97 60 105.91 60 107.20 59	01.28 54	.00 054.80 .91 654.81 .11 654.61				4	14.91 5 14.72 5 17.33 5
9/13/2010 8/23/2010	89.51 598.5	6 107.33 604. 6 107.24 605. 1 107.10 605.		586.07	113.31 5	586.96 587.11	75.23 58	84.47 9	97.12 97.06	581.28	96.40 96.20	581.50	84.31 84.16			566.22	93.43 93.21	576.57	52.80 52.42 52.21	649.73	89.34 (89.17 (621.08		600.26 10	09.34 596.0 09.17 596.2	7 64.11 4 64.06	613.97		620.81	107.10 60 107.05 60	00.09 55	.06 654.66 .03 654.69				4	17.16 50
8/19/2010 8/13/2010	89.13 598.9		31 70.11	586.39	113.09 5	587.18 590.47	75.08 58	84.62 9	97.03 36.28	581.37	96.10	581.80 584.73	84.09		12.03	566.37		576.90	52.11 52.00	650.04 650.15	89.80	620.62	107.00 6 100.00 6	600.36 10			614.05	44.04	621.06	107.00 60 98.43 60	00.19 55	.00 654.72 .41 676.31				4	17.03 50 18.77 50
8/6/2010 7/30/2010	90.41 597.6	6 108.54 603. 5 108.79 603.	82 65.90 57 65.72	590.60	108.44 5	591.83 592.36	68.77 59	90.93 8	37.08 37.77	591.32	92.78 92.55	585.12	82.85 82.71	579.85		564.19	90.11 87.49	579.89	51.69 51.25	650.46		620.57	99.12 6 97.41 6	608.24 10	04.81 600.6 04.29 601.1	0 57.81 2 56.21	620.27	45.51	619.59	98.12 60 97.63 60	09.07 31	.41 678.31 .46 679.26				4	18.25 50 18.16 50
7/23/2010 7/9/2010	94.88 593.1	9 107.44 604. 6 108.37 603.	92 64.97 99 64.85		107.86 5 107.34 5	592.41 592.93	67.56 59 66.98 59		38.36 38.65	590.04	92.23 92.08	585.67	82.61 82.53	580.09 580.17	13.11 12.81	565.29 565.59	86.48 84.13	583.52	50.74 50.69	651.41 651.46	89.75 (620.67	96.15 6 94.47 6	611.21 10	03.69 601.7 03.37 602.0	2 55.41 4 53.61	622.67	44.23 43.71	620.87 621.39	97.34 60 96.68 61	09.85 29	.14 680.58 .71 682.01					17.25 50 16.85 50
6/25/2010 6/18/2010	94.27 593.8	0 108.11 604. 6 108.52 603.		591.79		593.05	66.46 59 66.77 59	93.24 8	38.95 39.11	589.45	91.81 91.22	586.09	82.23 82.12	580.47 580.58	11.73 10.41		83.13 82.12	586.87	50.51 50.24	651.64		620.73		613.71 10	02.78 602.6 02.15 603.2	3 52.46 6 51.52	625.62	42.44 41.41		96.12 61 95.92 61	11.07 26	.41 <u>683.31</u> .42 <u>684.30</u>				4	45.11 5
6/11/2010 6/4/2010	103.72584.3104.11583.9	5108.47603.6108.69603.	8964.326764.91	592.18 591.59	106.22 5 105.62 5	594.05 594.65	66.835966.5159		39.27 1 39.31 1		91.88 92.23	586.02 585.67	82.41 82.55	580.29 580.15	10.98 11.53		85.41 86.12	583.88	50.19 50.23	651.96 651.92	89.44 (92.64 6 92.57 6		02.68 602.7 02.13 603.2	3 57.86 8 58.21		43.21 46.74		95.68 61 95.47 61		.89 <u>683.83</u> .71 <u>684.01</u>					15.11 5 17.45 5
5/28/2010 5/21/2010	106.84581.2104.71583.3	3108.71603.6111.22601.	6565.211465.17	591.29 591.33		595.42 595.39			39.88 38.77		92.18 91.84	585.72 586.06	82.68 82.55	580.02 580.15	11.71 10.86	566.69 567.54	87.81 87.37		50.21 49.81	651.94 652.34			92.41 6 92.77 6			4 59.51 7 58.79			616.59								46.85 50 46.13 50
5/14/2010 5/7/2010		4 112.85 5 99.	25 64.44 51 65.77	590.73	105.22 5		67.71 59	91.99 8	38.25 37.44	590.96	91.88 91.54	586.36	82.71 82.44	579.99 580.26	9.79	568.61	87.17 87.23	582.77	49.86 50.14		89.67 (620.75	92.65 6 92.97 6	614.39 10	00.37 <u>605.0</u>	4 58.44 4 57.92	620.16	48.21	616.89							4	15.97 5 15.61 5
4/30/2010 4/23/2010	92.86 595.2	6 112.81 599. 1 113.77 598.	5564.115964.88	591.62	105.66 5	595.86 594.61	66.41 5 9	93.29 8	37.21 8 35.77 8	592.63	90.77 90.41	587.13 587.49	82.71	580.13 579.99	7.19		88.77 88.79	581.21	50.33 50.16	651.99		621.09		614.50 9	99.23 606.1 98.55 606.8	8 57.77 6 57.23	620.85	49.67	615.43							42	14.78 50 12.96 50
4/16/2010 4/9/2010	87.91 600.1	2 114.22 598. 6 115.21 597.		591.83	107.42 5	593.38 592.85	67.66 59	92.04 8	34.61 4 34.65 4	593.75	89.73	588.19 588.17	83.11	579.53 579.59	7.44	570.96	89.55	580.45	49.57 49.55	652.58 652.60	89.22 (621.20	92.17 6 92.14 6	615.22 9	07.93 <u>607.4</u>	2 58.41 8 51.22	626.86	50.23	614.87							4	1.83 5 0.44 5
4/2/2010 3/26/2010	88.17 599.9	6 116.68 595. 0 116.71 595.		591.72	110.73 5	589.58 589.54	67.91 59	91.79 8	34.61 34.58	593.82	90.11	588.13 587.79	84.12	578.58	8.14	570.26	90.61	579.39	49.64 49.77	652.38		621.01		615.47 9		8 57.88 0 57.79	620.29	50.88	614.22							4	40.23 5 40.91 5
3/19/2010 3/12/2010 3/5/2010		<mark>6</mark> 117.11 <u>595</u> .	2 <mark>5</mark> 65.41	591.37 591.09	110.91 5	589.56 589.36	68.33 5 9		34.71	593.69	91.77	586.99 586.13	84.85	577.89 577.85	8.11		91.21	578.79	49.21 49.17	652.94 652.98	89.52 (620.90	U	615.09 9	8.11 607.3	7 57.86 0 58.41	619.67	51.44	613.66							4	11.88 50 12.13 50 10.77 50
3/5/2010 2/26/2010 2/19/2010		7 122.10 590. 3 121.94 590. 6 121.57 590.	42 66.72			589.15 588.33 588.36	69.42 59	90.28 8	35.82 36.91 39.11	591.49	92.71	585.35 585.19 584.96	84.36	576.88 578.34 578.93	8.54	570.25 569.86 569.63	91.45 90.92 90.13	579.08	49.20 48.95 48.81	652.95 653.20 653.34	84.11 (626.31	92.30 6 97.11 6 92.27 6	610.25 9	08.20 607.2 08.76 606.6 08.11 607.3	1 60.31 5 61.77 0 62.41	616.31	51.88	613.22							4	10.77 5 12.11 5 12.77 5
2/19/2010 2/12/2010 1/29/2010		0 120.42 591.	68.21	588.29		587.50	71.13 58	88.57 9	91.18	587.22	93.55	584.35	83.55	578.93 579.15 580.07	8.99	569.41	89.77	580.23	48.88	653.27	74.13 (636.29		614.82 9	8.11 607.3 98.21 607.2 98.54 606.8	0 65.23	612.85	49.67	615.43							4	12.49 50 16.51 50
1/22/2010 1/22/2010 1/15/2010		6 120.85 5 91.	51 68.91	587.59	112.81 5 112.86 5 112.90 5	587.41	71.23 58		91.81	586.59	93.79		82.77	579.93	9.15		88.71	581.29			66.41 (644.01		614.59 9	8.77 <u>606.6</u>	4 65.91	612.17		615.97							4	12.44 5 12.36 5
12/18/2009 12/11/2009	101.80 580.2 103.47 584.6 103.81 584.2	0 122.72 589.	<mark>64</mark> 71.33	585.17	114.21 5	586.06 585.46	72.69 58		95.37	583.03	96.11	581.79		580.76	10.22	568.18	93.23	576.77 574.43	50.23	651.92	68.12 (642.30	92.11 0 95.91 6 96.51 6	611.45 10	06.92 598.4	9 65.82	612.26		614.55							4	16.22 50 16.11 50
12/4/2009 11/27/2009	103.60 584.4 107.11 580.9	7 121.45 590.	91 72.00	584.50	115.83 5	584.44 583.06	73.57 58		97.45	580.95	97.11	580.79	83.68	579.02	11.81	566.59	98.41	571.59	52.20	649.95 646.84	87.60 (622.82	98.60 6 102.91 6	608.76 1 ⁻	12.00 593.4	1 66.88	611.20 611.54	52.88	612.22							4	16.27 50 16.54 50
11/13/2009 11/6/2009	103.21 584.8			586.27	113.96 5	586.31 587.27	67.48 59	92.22 9		581.18		580.56		577.79	10.41	567.99 566.44		572.79		646.82		621.01	102.41 6	604.95 10	04.71 600.7 04.81 600.6		611.31	47.33	617.77							4	16.23 50 18.53 50
10/30/2009 10/23/2009	92.11 595.9	6 101.48 610. 4 104.31 608.	8867.910568.96	588.59 587.54	101.96 5	598.31 597.17	66.52 <mark>5</mark> 9	93.18 9	97.29 97.43	581.11	97.72 97.55	580.18	86.21 86.71	576.49	12.11		97.11	572.89	53.58 54.42	648.57 647.73	89.49 (620.93		607.98 10	04.21 <u>601.2</u> 01.96 <u>603.4</u>		613.71	47.31	617.79							4	18.21 56 17.51 56
10/19/2009 10/16/2009	93.41 594.6 97.40 590.6	6 104.92 607. 7 105.65 606.	4466.437168.72	590.07 587.78	103.91 5 104.35 5	596.36 595.92	NM 69.96 58	NM 89.74	NM 95.50	NM	NM 95.10	NM 582.80	NM 85.02	NM 577.68	NM 10.85	NM 567.55	NM 93.30	NM 576.70	54.26 54.31	647.84	89.89 (89.80 (620.53 620.62	102.11 6 101.58 6	05.25 05.78		NM 63.71	NM 614.37	NM 44.53	NM 620.57							4	NM 4.78 56
10/15/2009 10/14/2009	92.11 <u>595.9</u> 92.37 <u>595.7</u>	6105.72606.0105.80606.	68.72	587.62 587.78	104.31 5	595.82 595.96	NM	NM	NM NM		NM NM	NM NM	NM NM	NM NM	NM NM	NM NM	NM NM	NM NM	54.41 54.79	647.74 647.36	89.63 (89.69 (620.79 620.73	101.92 6 102.00 6	605.44 605.36		NM NM	NM	NM NM	NM								NM NM
10/13/2009 10/12/2009	94.23 593.8		68.58	587.92	101.00 5 NM		NM	NM	NM	NM	NM NM	NM NM	NM NM	NM NM	NM NM	NM	NM NM	NM	55.57	646.58	88.61 (621.81	64.71676.416	30.95		NM NM	NM NM	NM	NM								NM I
10/9/2009 10/7/2009	94.10 593.9 69.71 618.3	6 115.37 <u>596</u> .	26 68.18 99 68.19	588.31	NM NM			NM		NM	94.62 NM	NM	84.13 NM	578.57 NM	NM	568.78 NM	NM	NM	74.21 58.86	627.94 643.29	94.22 (616.20	58.24 6 54.44 6	52.92		NM	NM	38.31 NM	NM								14.33 56 NM
10/6/2009 10/2/2009	98.41 589.6	4 105.67 606. 6 106.71 605.	69 65.34 65 68.28	588.22				90.29 9				NM 583.24						575.28	61.58 61.71	640.57 640.44			82.44 6 82.88 6			NM 64.71	NM 613.37										NM NM
9/23/2009 9/18/2009	92.38 595.6 100+ NM	100+ NN	67.71	588.79	NM		•••••	91.82 9	94.58	584.12	94.38	583.79	85.56 85.57	577.13	12.77	567.12 565.63	93.41	576.59										45.81	617.29 619.29								
8/27/2009 8/20/2009	NM NM 71.44 616.6	100+ NM 3 92.51 619.		589.13 607.99			67.585947.7767	92.12 9 11.93 8						577.54 588.48															617.48 620.38								

= Seasonal low water levels.

PLATE 1 GROUND WATER LEVELS 2009-2011 Hanson Aggregates New York LLC Alpha Project No. 11110

APPENDIX A

NYSDEC Well Completion Reports

NEW YO	RK STATE DEPARTMENT OF ENVIROI	MENTAL CONSERVATION	Å
(1) county Livingston		(3) DEC Well Number	LV943
(2) Township Lima	WELL COMPLETION REI	PORT	
(4) OWNER	Perese Traver		LOG *
(5) ADDRESS 1149 Datton		11/11/20 10 1	708 ft. above sea level
(6) LOCATION OF WELL (See Instructions On Reverse Show Lat/Long if available and method used: 042°576′6, (□ GPS □ DEC Website A Map Interpolation	"1149 Dalton Rd 66"N 07703718	Top Of Casil ft.above (+) of	ng is located or below (-) ground surface
(7) DEPTH OF WELL BELOW LAND SURFACE (Feet) 12-0 /	(8) DEPTH TO GROUNDWATER BELOW LAND SURFACE (Feet)	DATE MEASURED	TOP OF WELL
	A CASING STATES AND A CASING AND A		
(9) DIAMETER 6 In.	in. in.	in	
(10) LENGTH ft.	ft. ft.	in.	
(11) GROUT TYPE / SEALING	(12) GROUT / SEALING INTERVAL (Feet) FROM	то	
(13) MAKE & MATERIAL	(14) OPENINGS		2 0 vt 55 ft Ned 120') 5 to 65'
(15) DIAMETER in.	in. In.	in.	10456 pt
(16) LENGTH ft.	n. n. .	in allans	
(17) DEPTH TO TOP OF SCREEN, FROM TOP OF CA	SING (Feet)		10
	71. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	den	5
(18) DATE	(19) DURATION OF TEST	, lfr.	
(20) LIFT METHOD	(21) STABILIZED DISCHARGE (GPM)		
(22) STATIC LEVEL PRIOR TO TEST (feet/inches below lop of casing)	(23) MAXIMUM DRAWDOWN (Stabilized) (feet/inches below top of casing)	1	highly
(24) RECOVERY (Time In hours/minutes)	(25) Was the water produced during test discharged away from Immediate area? Ye	s No	fractured
aŭ	MEINSTANDALION		
(26) PUMP INSTALLED? YES NO (27) D	ITE (28) PUMP INSTALLER		-100'
(29) TYPE	KE (31) MODEL		Limestone + Shale
(32) MAXIMUM CAPACITY (GPM)	(33) PUMP INSTALLATION LEVEL FROM TOP OF CASING (Feet)	\	* Shale
(34) METHOD OF DRILLING CLECONOUT	d (35) USE OF WATER (see instructions for choices) bome	stic	
(36) DATE DRILLING WORK STARTED	(37) DATE DRILLING WORK COMPLETED		
	m K Moraver -	REGISTRATION NO.	
1-126/01 Ba	rney Moravectic 11	2024	1000
beds and water levels in each; casings	ntered with depth below ground surface, v ; screens; pump; additional pumping test sulphur, salt, methane). Describe repair	s and other BC	DTTOM OF HOLE
See further instructions titled "Instructions	ons for New York State Well Completion F	Report". NYS	DEC COPY

E

NE	W YORK	STATE DEPART	MENT OF ENVIRO	NMENTAL CONS	ERVATION	
(1) County Livingston (2) Township Lima				(3) DEC W	Veli Number	LV 798
(2) Township <u>Chill</u>	W	ELL COMP	PLETION RE	PORT		
(4) OWNER SCOH + A	my	Koch				LOG *
(5) ADDRESS 199 Vikin	nqu	24 Bro	ickport 1	14420 VY	Ground Surface EL.	661 ft. above sea level
(6) LOCATION OF WELL (See Instructions Or Show Lat/Long if available and method used: 042°576 □ GPS □ DEC Website √ Map Interpola	'35.5	Salton (9«N 07	20 3716.0	65"W	Top Of Casin ft.above (+) o	g is located r below (-) ground surface
(7) DEPTH OF WELL BELOW LAND SURFACE (Feet)	<u>کر</u>	(8) DEPTH TO GROL BELOW LAND SU	JNDWATER JRFACE (Feet)	DATE MEASURED		TOP OF WELL
			han a san an a			
(9) DIAMETER	in.		in.	in.		clay
(10) LENGTH	ft.		π.	in.		3
(11) GROUT TYPE / SEALING		(12) GROUT / SEALII (Feet)	NG INTERVAL FROM	то		sand
(13) MAKE & MATERIAL		(14) OPENINGS		lises mis Yasar Ma		Compact
(15) DIAMETER	ín.	<u> </u>	in.	in.		
(15) LENGTH ft.			ft.	in.		Gravely
(17) DEPTH TO TOP OF SCREEN, FROM TO	P OF CASING	(Feet)				+ill +
	kozekte ()	10520 (Shadey				-39'
(18) DATE 8/2/02		(19) DURATION OF 1	30 mir)		
(20) LIFT METHOD	🗆 Bail	(21) STABILIZED DIS	CHARGE (GPM) 75			
(22) STATIC LEVEL PRIOR TO TEST (feet/inches below top of casing)		(23) MAXIMUM DRAV (feet/inches below				Limestone
(24) RECOVERY (Time in hours/minutes)		(25) Was the water pr discharged away	oduced during test from immediate area? Ye	es No		
(26) PUMP INSTALLED? YESNO	(27) DATE		(28) PUMP INSTALLER			
(29) TYPE	(30) MAKE		(31) MODEL			
(32) MAXIMUM CAPACITY (GPM)		(33) PUMP INSTALLA FROM TOP OF C				
		MARS SECTION	SOUTH SECONDERVI	NARE PROVIDENT		
(34) METHOD OF DRILLING		(35) USE OF WATER (see instructions f	or choices)	estic		
(36) DATE DRILLING WORK STARTED		(37) DATE DRILLING				
(38) DATE REPORT FILED	(39) DRILLER	R& COMPANY	(40) DE(REGISTRATION NO.		
8/14/02	Jonr	$h K \cdot n o $	ravectic	10024		
* Show log of geologic materials	encountere	d with depth belo	ow ground surface,	water bearing		1 - 150'
beds and water levels in each; or matters of interest, e.g., water q separate sheet if necessary.	asings; sc uality (sulp	reens; pump; add hur, salt, methan	ditional pumping tes ie). Describe repai	ts and other r work. Attach	BO	TTOM OF HOLE
See further instructions titled "In	structions t	or New York Sta	te Well Completion	Panot	NYS	DEC COPY

W

NE	W YORK	STATE DEPAR	TMENT OF ENVIRO	ONMENTAL CON	SERVATION	
(1) county Livingston				(3) DEC V	Vell Number	LV874
(2) Township Lima	W			PORT		
(4) OWNER Lori Kloc						LOG *
(5) ADDRESS 1168 Dalton	Rd,	Honeo	ye Falls	NY 14472	Ground Surface EL.	69 ft. above sea level
(6) LOCATION OF WELL (See Instructions Or Show Lat/Long if available and method used: 04-2.0 □ GPS □ DEC Website Map Interpole	ation	168 ba 21.46"N	1ton Ro 077°37'	l 21.98"W	Top Of Casing	is located below (-) ground surface
(7) DEPTH OF WELL BELOW LAND SURFACE (Feet)	, '	(8) DEPTH TO GRO BELOW LAND S	UNDWATER SURFACE (Feet)	DATE MEASURED	8-2	OP OF WELL
(9) DIAMETER	in.		in.	in.	ob	Glacial
(10) LENGTH 78 ft.	ft.		ft.	in.	whole	Glacial till- fewel str
(11) GROUT TYPE / SEALING Dentanitehole ((12) GROUT / SEAL (Feet)	ING INTERVAL	то <u>30'</u>	l de J	grave
(13) MAKE & MATERIAL		(14) OPENINGS			je sz	-50
(15) DIAMETER	in.		in.	in.	= 84	
(16) LENGTH ft .	t.		ñ.	in.	1 × 2	
(17) DEPTH TO TOP OF SCREEN, FROM TO		(Feet)			$\int \cdot x f$	Linestone
(18) DATE 6/16/03		(19) DURATION OF	^{TEST} 30 m i	\sim	is the	
(20) LIFT METHOD	🗆 Bail	(21) STABILIZED DIS	SCHARGE (GPM)	2+	Sas	
(22) STATIC LEVEL PRIOR TO TEST (feet/inches below top of casing)		(23) MAXIMUM DRA (feet/inches belo	WDOWN (Stabilized) w top of casing)		5 33	
(24) RECOVERY (Time in hours/minutes)			· · · · · ·	es No	r de la	
(26) PUMP INSTALLED?	(27) DATE		(28) PUMP INSTALLER		L L L	
YES NO (29) TYPE	(30) MAKE		(31) MODEL		e e e e	bertie
(32) MAXIMUM CAPACITY (GPM)	I	(33) PUMP INSTALL FROM TOP OF C	ATION LEVEL CASING (Feet)		hola hola	Bernie
(34) METHOD OF DRILLING		(35) USE OF WATER			र देवे,	0
Rotary Cable Tool Other		(see Instructions		stic	FR3	5 - 150
(36) DATE DRILLING WORK STARTED			WORK COMPLETED		e porto	Nomite
(38) DATE REPORT FILED 7/25103		K. Mora	IVEC ! .	0024	t à	Dolomite
 Show log of geologic materials e beds and water levels in each; c matters of interest, e.g., water qu separate sheet if necessary. 	encountere asings; sci	d with depth beli eens; pump; add	ow ground surface, ditional pumping tes	water bearing	E n E BOT	TOM OF HOLE
See further instructions titled "Inst	structions f	or New York Sta	te Well Completion	Report".	NYSD	EC COPY

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NYOUEUU T

(1) county LivingSton				(3) DEC V	Vell Number	LV951
(2) Town LIMA	W	ELL COM				
(4) OWNER DAUCD FE	arrov			<u> </u>		LOG *
(5) ADDRESS	<u>Λ</u>	, , , , , , , , , , , , , , , , , , , ,	Juno Julio	111/72	Ground	
(6) LOCATION OF WELL (See Instructions On	M Ka	a Mon	usye talls	14472	Surface EL.	ft. above sea level
Show Lat/Long if available and method used: GPS DEC Website Amap Interpolat	115	o Dalto	n Rd Ho	whe Jale	Top Of Casing ft.above (+) or	below (-) ground surface X
(7) DEPTH OF WELL BELOW LAND SURFACE (Feel)	, ,	(8) DEPTH TO GRO BELOW LAND S	UNDWATER URFACE (Feet)	DATE MEASURED	Т	OP OF WELL
(9) DIAMETER		ASINGS	jn.	in.		H D'-1' BEALL
(10) LENGTH	ft.	 	ft.	in.		Clay
(11) GROUT TYPE / SEALING		(12) GROUT / SEAL (Feet)	ING INTERVAL FROM	то	201	
(13) MAKE & MATERIAL	S SAC	REENS			of.	1~150
				5. ,,	Casura	Sing
(15) DIAMETER	in,		in.	in.		
(16) LENGTH (t.	ft.	1	ft.	ln.		Delamite
(17) DEPTH TO TOP OF SCREEN, FROM TOP	OF CASING	(Feet)				
(18) DATE		(19) DURATION OF	STRUCK CONTRACTOR AND CONTRACTOR AND CONTRACTOR OF A DESCRIPTION			
(20) LIFT METHOD		(21) STABILIZED DIS	SCHARGE (GPM)			
□ Pump □ Air Lift (22) STATIC LEVEL PRIOR TO TEST	O Bail	(23) MAXIMUM DRA	WDOWN (Stabilized)			
(feet/inches below top of casing) (24) RECOVERY (Time in hours/minutes)	! -	(feet/inches belo	w top of casing)			
			from immediate area? Yes	No		
(26) PUMP INSTALLED? YESNO	(27) DATE		(28) PUMP INSTALLER			
(29) TYPE	(30) MAKE		(31) MODEL			
(32) MAXIMUM CAPACITY (GPM)		(33) PUMP INSTALL FROM TOP OF C				
(34) METHOD OF DRILLING Rotary Cable Tool Cother		(35) USE OF WATER (see Instructions	for choices) domes	tie		
(36) DATE DRILLING WORK STARTED		(37) DATE DRILLING 5-4	WORK COMPLETED			
_	(39) DENLER	Le Water L	well Drillers	EGISTRATION NO.		
5-17-04	net	ME URL	KE GWD NYR	D 10070		151
 Show log of geologic materials el beds and water levels in each; ca matters of interest, e.g., water qu 	asings; sci	eens; pump; ad	ditional pumping tests	and other	BOT	TOM OF HOLE
separate sheet if necessary.					NVSI	

W

COUNTY MONYOE				(3) DEC V	Vell Number
TOWN RUSH				<u>moi</u>	740
4- OWNER	ATER WELL	COMPLETION	KEPORI		
wayne Pluta				⁽⁴³⁾	.OG
SLACDRENS			D	epth to Bedrock	(ft. below
6) LOCATION OF WELL (See Instructions On Reverse)		as address above, also provide	Lat / Long below) C	Ground Elev. 674	ft. above S.L.
Show LauLong if available 525 WOV K	is Rd			op of Casing	
GPS Map Interpolation 42° 57 · 3					w (-) ground surface
LAND SURFACE (feet)	(8) DEPTH TO GRO BELOW LAND S		DATE MEASURED	1000	F WELL
a thame ten	CASINGS				
6 in.	in.	in.	in.		
IG) LENGTH ft.	ft.]	ft.	ín.		
11) GROUT TYPE / SEALING	(12) GROUT / SEAL (feet)		ro		
		he Helicide in the short of the	Ani andre Setter		
(3) MAKE & MATERIAL	(14) OPENINGS				
	ìn,	in.	in.	ζ	
No. THE TH		1		2	
ft.	ft.	ft.	in.		
				}	
(18) DATE	YIELD TEST	rtest		60	
4123/09		<u>90 mir</u>	2	ξ	
20) LIFT METHOD Pump X Air Lift Bail	(21) STABILIZED D	ISCHARGE (GPM) 30+		2	
STATIULEVEL PRIOR TO TEST dereaches below top of casing)		AWDOWN (Stabilized) low top of casing)		5 1	
24) RECOVERY (Time in hours/minutes)	(25) Was the water discharged awa	produced during the test by from immediate area? Yes	No	2 l	
PU				· -	
261 PUMP INSTALLED?YESNO	(27) DATE	(28) PUMP INSTAL	and the second state of the second state of the	7 5	
29) TYPE	(30) MAKE	(31) MODEL		D -	
	(33) PUMP INSTALI			361	
	FROM TOP OF	CASING (Feet)		9 -	
WYCTHORDE DRILLING CLEANOUT	(35) USE OF WATE	•	,	89	
Rotary Cable Tool Othe Deepen		G WORK COMPLETED	tic !!	pac	
9/23/09		9123109		38	
38) DATE REPORT FILED (39) REGISTERED COMPANY 9/29/09 D	((40) DEC REGISTRA		fre	
barney 1	loravec.	Inc NYRD	10024	35	
U) CERTIFIED DRILLER (Print name)				-	
David S. Moravec	her	ra		1	1
By signing this document I hereby affirm that defined by Environmental Conservation Law §1:	: (1) I am certified to s 5-1502; (2) this water	supervise water well drilling well was constructed in acc	activities as	BOTTOM	OF HOLE
water well standards promulgated by the New Y	York State Department	of Health; (3) under the p	enalty of		
perjury the information provided in this Well Co	moletion Report is true	 accurate and complete in 	nd I	A 13 / A	C COPY

(1) COUNTY MONTOE			Γ	(3) DEC V	Vell Number
(2) TOWN Rush				mo	1741
	TER WELL CO	MPLETION REPORT	Ļ		
Wayne Pluta			_	⁽⁴³⁾ L	.OG
1525 MONTHS RA H	oneoye Fo	UIS NY 14472	Depth	to Bedrock	(ft. below
(6) LOCATION OF WELL (See Instructions On Reverse) (Ch	eck here 🔄 if same as addre	ess above, also provide Lat / Long below)	Groun	d Elev.	ground surface) <u>3</u> (ft. above S.L.)
Show LaULong if available Honeoye Fal			Top of		(ft., above (+)
(7) DEPTH OF WELL BELOW	6/ N 77 (8) DEPTH TO GROUNDWA	<u>38' 1.26' W</u>			w (-) ground surface)
LAND SURFACE (feet)	BELOW LAND SURFACE	E (feet)	-		
(9) DIAMETER	<u>نىتى. مىنى نى بارىمى ئى بارىمى مىنى بارىمى مىنى مىنى مىنى مىنى مىنى مىنى مىنى </u>	inder and the state of the second s	-		
(10) LENGTH	in.	in. in.	-	,	
ft.	ft.	ft. in.		A	
(11) GROUT TYPE / SEALING	(12) GROUT / SEALING INT (feet)	FROMTO	n [n	
(13) MAKE & MATERIAL	(14) OPENINGS	Yang lightang altigraph market		n	
(15) DIAMETER in.	in.	in, in,		र २	
(16) LENGTH ft.	ft.	ft. in.	5		
(17) DEPTH TO TOP OF SCREEN, FROM TOP OF CASING (Feet)				1	
	ELD TE\$T				
(18) DATE 9/24/09	(19) DURATION OF TEST	zhrs.	7	5	
(20) LIFT METHOD Pump X Air Lift 🔲 Bail	(21) STABILIZED DISCHAR		-	$t \dot{o}$	
(22) STATIC LEVEL PRIOR TO TEST (feet/inches below top of casing)	(23) MAXIMUM DRAWDOW (feet/inches below top o		-	1 00 4	
(24) RECOVERY (Time in hours/minutes)	(25) Was the water produced discharged away from in			2	
PUNP	NSTALLATION	的现在分词,如此 如此的	92 -	F	
(26) PUMP INSTALLED? YES NO	(27) DATE	(28) PUMP INSTALLER	9	2 -	
(29) TYPE	(30) MAKE	(31) MODEL		- A	
(32) MAXIMUM CAPACITY (GPM)	(33) PUMP INSTALLATION I FROM TOP OF CASING				
	متحد فبكر والكناف والمتحدث ويترفع ويتغرب والمتحا فالمتك وترتب وتكفيه والمتحربين والتجرب والمحد	il and it is such a second second		12	
(34) METHOD OF DRILLING CLEANOUT	(35) USE OF WATER (See instructions for cho	101100			
(36) DATE DRILLING WORK STARTED	(37) DATE DRILLING WORK	COMPLETED]		
(38) DATE REPORT FILED (39) REGISTERED COMPANY 9/29/09 Days and the second	oravec Inc	(40) DEC REGISTRATION NO. NYRD 10024			
(41) CERTIFIED DRILLER (Print name)	(42) CERTIFIED DRILLER S	and a second	-1		
David S. Moravec	17/201	Ale -			
* By signing this document I hereby affirm that: (1) defined by Environmental Conservation Law §15-15	i02; (2) this water well w	as constructed in accordance with		BOTTON	OF HOLE
water well standards promulgated by the New York perjury the information provided in this Well Compl understand that any false statement made herein is §210.45.	etion Report is true, accu	rate and complete, and I	N	YSDE	ССОРУ

(1) COUNTY MONYOE (2) TOWN RUSH					ell Number
	ATER WELL	COMPLETION F	REPORT	mor	142
(4) OWNER Wayne Pluta				⁽⁴³⁾ L	OG
(5) ADDRESS 525 Works Rd		je Falls N	9	pth to Bedrock	(ft. below ground surface)
(6) LOCATION OF WELL (See Instructions On Reverse) (Show Lat/Long if available and method used:	Check here ∏ if same as Ye Falls	s address above, also provide I + 6 Rd	0,	•	【(ft. above S.L.) (ft., above (+)
GPS X Map Interpolation 42° 56' 4	The second se				(-) ground surface)
(7) DEPTH OF WELL BELOW LAND SURFACE (feet)	(8) DEPTH TO GROU BELOW LAND SU		ATE MEASURED	TOP OF	WELL
	CASING8		-	5	
(9) DIAMETER 6 in. 1	in.	in.	in.	$\frac{1}{2}$	clay
(10) LENGTH 40 ft.	ft.	ft.	in.	by I	
Bentonite	(12) GROUT / SEALIN (feet)	FROM T		32	-5'
(13) MAKE & MATERIAL	(14) OPENINGS	adostradas de la sua		Å	
(15) DIAMETER	in.	in.	in.	0	Limesto
(16) LENGTH ft.	ft.	ft	in.	25	Lime
(17) DEPTH TO TOP OF SCREEN, FROM TOP OF CASING (Fe	eet) .			-R	
	YIELD TEST		1	ξ σ	
(18) DATE 9/27/00	(19) DURATION OF T	and seeing - and a second s		2×	
(20) LIFT METHOD X Pump Air Lift Bail	(21) STABILIZED DIS		(N 20	
(22) STATIC LEVEL PRIOR TO TEST (feet/inches below top of casing)	(23) MAXIMUM DRAV (feet/inches belo	WDOWN (Stabilized)		U S	
(24) RECOVERY (Time in hours/minutes)		oduced during the test from immediate area? Yes	No	53	
	PINSTALLATION		it is a part of the		
(26) PUMP INSTALLED? YES NO	(27) DATE	(28) PUMP INSTAL	LER	22	
(29) TYPE	(30) MAKE	(31) MODEL		33	
(32) MAXIMUM CAPACITY (GPM)	(33) PUMP INSTALLA FROM TOP OF C			$\Delta \xi$	Broke Up i mestor
and the second	Lasure of water	ويتوادون ومسادية ويستعربون ومعين والمتعصر والمحال فالمتعادين والمحاد والمتعادية والمتعادي المحاد	iceschichijit.	3 21	00
(34) METHOD OF DRILLING Cable Tool Other (36) DATE DRILLING WORK STARTED		(or choices) Domest	ic e	8 3	inesto
(38) DATE REPORT FILED [39) REGISTERED COMPANY	(ST) DATE DRILLING	912309		a R	L
9/29/09 Barney M	oravech		0024	Jer	
David S. Moravec	(42) CEBTIFIED DRIL		0	20	
		popuíse wotor well drillion	activities as	ı	I
* By signing this document I hereby affirm that: defined by Environmental Conservation Law §15- water well standards promulgated by the New Yo perjury the information provided in this Well Com understand that any false statement made hereir	1502; (2) this water v ork State Department o upletion Report is true,	vell was constructed in acc of Health; (3) under the pe accurate and complete, ar	ordance with enalty of nd I	BOTTOM NYSDE(
§210.45.	1		8/2007		

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NEW YORK STATE DEPARTMENT OF ENVIRONMENTAL CONSERVATION

AIR

HOUNTY MONTOR			(3) DEC Well Nu	mber
JWN RUSH W	ATER WELL COMPLET	ON REPORT	MOITS	e
Lowner Lon Knab Address		14477	⁽⁴³⁾ LOG	
1855 Honeoye Falls 6-LOCATION OF WELL ISOE Instructions On Reversed as Show LakLong if available	$5 \pm 6 Rd$ Honeoy Check here Will same as address above, also	CFULSNY provide Lat 'Long below) Gr	epth to Bedrockgrou grou ound Elevift.	ind surface,
GPS X Map interpolation 42° 56' 4	7.58"N 77° 38	29.53"W	p of Casing(f or below +-) gro	
T DEPTH OF WELL BELOW LAND SURFACE (feet)	(8) DEPTH TO BROUNDWATER BELOW LAND SURFACE (feet,	DATE MEASURED	TOP OF WEL	L.
9. DIAMETER	CASINGS			
b in L.	in in.	in C	2	
ft	ft ft	in. -	-	
Sealing	(12) GROUT DEADING IN "ERVAL (feet) FROM	TO	$\rho_{\rm I}$	
	SCREENS			
TH DAKE & MALERIAL	(14) OPENING'S		-	
···· DIAMETER	in. In Internet	in 🖌	5	
LIG ENGTH ft.	ft	ιn		
PROPERTY TO TOP OF SCREEN FROM 1:0P OF CASING (F	ð!.		ن ا	
//	PIELD TEST		2	
13-DATE 12/16/09	(19) DURATION OF TEST	min		
	(21) STABILIZED DISCHARGE (GPM)			
-21-STATIC LEVEL PRIOR TO TEST - feet increasibelow for of casing)	(23) MAXIMUM DRAWDOWN (Stabilized) (frietinche - selow top of casino)		ゼ ゴ	
-24) RECOVERY (Time in hours/nimutos)	(25) Was the willer produced during the test discharged away from immediate area?		5	
PUM	PINSTALLATION	<u> </u>	4	
	(27) DATE (26) PUI			
NUM TYPE	12/16/09 J.C 301 MAKE 0 1311 MO	lorave -		
	133) PUMP INSTALLATION LEVEL	50 1422	d l	
77	FROM TOF OF CASINE STREES	75	ξ II	
Statue DE DRILLITES Cleanert Idee per	Security Decision		S I	
8 - ORIE DRIELING WORK STAFTED	STEDATE DRIE NE UNITY COMPLETED	mestic :	チート	
121609 CONSTRUCTION RECORDED COMPANY	12/16/09 140) DEC	REASTRATION NO	ଧ	
1/8/10 Barney M	NYF	10024	Ke	
11 CERTIFIED DRILLER (Print name)	142) CERTIFIEC DRILLER SIGNATURE			
John K. Moravec	Al Al Com		→	
 By signing this document Thereby affirm that: refined by Environmental Cours rivation Law §15 	1502, (2) this water well was construct	ed in accordance with [BOTTOM OF H	OLE
solater well standards provided of the New Ys projury the information provided in this Well Con conceptand that imy faller starters of model heater \$210.45.	pletion Report is how, an mate and con-	iplote, and 1 modes Period Law	NYSDEC C	OPY

APPENDIX B

Logs of Fractures in Core by Alpha Geoscience

	Alpha Geoscience 679 Plank Road Ce Clifton Park, New York 12065	FRACTURE LOG	Boring ID: DDH 1-02 Page 1 of 2
Project I	Number/Name: 11110/ Hanson Honeo	ve Falls Location: Honeoye	e Falls, NY
Drilling	Contractor/Personnel: NA		
Geologi	ist/Inspector: Steve Trader (Fracture		Start/ 6-26-02 (coring) Finish Date: 6-26-02
Drilling	Equip/Method: NA	Core Diameter:	1 7/8"
Samplir	ng Method: Coring		Well Installed? No
Elevatio	on/Ground Surface: 705.8		A
Depth te	o Ground Water from Ground Surfac	e (Date): Not Measured	
REMAR		actures only - Geology logged separately in mmon; staining not present on fracture surfac	
Depth (Ft)		DESCRIPTION	
	 near vertical fracture 13.0' 18.0 to 18.2' angular fracture 22' angular fracture 27' angular fracture at end of ru Box 3 (28.3' - 37.8') 28.9' - near horizontal fracture at 29.4' - angular facture, weather 30.4' - small vug 33.3' - horizontal fracture/break 33.9' - angular fracture with pot 35.5' - near horizontal break wire core fragments at edges Box 4 (37.8' - 47.0') 43.7' core spin 47.0' core spin 57.0' core spin at end of run; 0 Box 6 (57.2' - 67.0') No apparent na Box 7 (67.0' - 76.8') No apparent na Box 8 (76.8' - 86.3') 78.5' Potential natural break al 	3' with no staining 11.3 - 11.4', with core spin at 11.4' - 14.0' (depths not certain due to poor recover pear drilling related, except: an; secondary mineralization on fracture surfated along chert nodule; with potential brownish stated appearance and apparently silt-filled. with grooved appearance to fracture surface ential iron staining; with angular stylolitic fract th weathered fracture surface and apparent c s. .1' of dried clay and rock fragments. atural fractures. atural fractures. atural fractures. ong thin packstone stylolitic interval; appears and also some dried clay/mud is present on fr more vuggy below 89.5'	ace with potential iron staining. aining. with potential iron staining. ture below (core not broken). lay-filling (dried now); missing
	Box 10 (96.0' - 104.7') Becoming m 101.8' - 102.1' several core bre natural fractures	ore coarsely crystalline and less vuggy. aks in this interval are uneven likely due to ab but no staining.	prasion during drilling, possibly

C	
ALPHA GEOSCIENCE	

FRACTURE LOG

Boring ID. DDH 1-02

Page 2 of 2

Project Number/Name: 11110/Honeoye Falls

Location: Honeoye Falls, NY

Depth (Ft)	DESCRIPTION
	Box 11 (104.7' - 114.5') 108.4' Core abrasion along fracture surface, but not core spin; no staining. 111.6' Core abrasion along fracture surface, but not core spin; no staining .
-	Box 12 (114.5' - 123.9') Core is a bit jumbled in the first few feet of this box. 116.6' - horizontal fracture, rough surface; with apparent reddish brown staining; core on either side of fracture does not fit perfectly well, but as if there was some separation.
-	Box 13 (123.9' - 130.5') 129.0' - 129.15' interval with dried mud and rock fragments (not at the end or beginning of the run) 129.7' - 130.0' (approx) - broken interval with chunks <1" diameter
	Box 14 (130.5' - 137.0' TD) No natural water bearing fractures
-	
-	
_	
-	
_	
-	

C	Alpha Geoscience 679 Plank Road	FRACTURE LOG	Boring ID: DDH 4-02				
ALPH GEOSCIEN	Page 1 of 1						
Project Number/Name: 11110/ Hanson Honeoye Falls Location: Honeoye Falls, NY							
Drilling	Drilling Contractor/Personnel: NA Start/ 6-29-02 (coring)						
Geologi	Geologist/Inspector: Steve Trader (Fracture log only) Finish Date: 6-29-02						
Drilling	Equip/Method: NA	Core Diameter: 1	7/8"				
Samplir	ng Method: Coring	We	ell Installed? No				
Elevatio	on/Ground Surface: 701.8						
	o Ground Water from Ground Surfac						
REMAR		ractures only - Geology logged separately in 200 mmon; staining not present on fracture surfaces					
Depth (Ft)		DESCRIPTION					
	0-21': unconsolidated overburden Box 1 (21' - 30.5') No apparent nat	ural fractures; core spin at very top of core at 21	Ч.				
	Box 2 (30.5' - 40') 33.2' angular fracture; abr	aded surface					
_	Box 3 (40' - 50') 47' core spin; abraded surfaces; horizontal						
	Box 4 (50' - 60') No apparent natural fracture						
	 Box 5 (60' - 70') 69.3' possible silt seam (dried); contact is slighted abraded, though pieces fit well, definitely not a fresh break; dried silt is not in place and is crumbled in box. 						
	 Box 6 (70' - 79.2') 0.1' thick, dried mud seam at 71.9' - 72.0'; also 1/2" thick, silt seam at 75.7' 						
	Box 7 (79.2' - 89') 82.9' core spin 84.9' abraded core break with dried mud and rock chips						
-	Box 8 (89' - 99') No apparent natur	al fracture; some vugs					
	Box 9 (99' - 109') No apparent natu	ıral fracture; small vugs					
	Box 10 (109' - 119') Apparent dried mud seam (0.1' thick) at 115' and at 115.25' (very thin)						
	Box 11 (119' - 129') 127.4' Core spin; break is abraded, with apparent dried mud seam.						
	 Box 12 (129' - 139') Edgecliff/Akron contact at ~137.3' is abraded; Akron has distinct petroliferous odor near vertical fracture (healed) from top of Akron (137.3') to 139' 						
-							
_	-						
_							

	Alpha Geoscience 579 Plank Road	FRACTURE LOG	Boring ID: DDH 4-98				
GEOSCIENCE	Clifton Park, New York 12065		Page 1 of 2				
Project Number/Name: 11110/ Hanson Honeoye Falls Location: Honeoye Falls, NY							
	Drilling Contractor/Personnel: NA Start/						
	nspector: Steve Trader (Fracture		sh Date: 1998				
	uip/Method: NA	Core Diameter: 1 7					
	Method: Coring	Wel	I Installed? No				
	Ground Surface: 705'						
	round Water from Ground Surfac	e (Date): Not Measured actures only - Geology logged separately in 199	8 by P. Griggs (Marshall)				
		mmon; staining not present on fracture surfaces					
Depth (F1)		DESCRIPTION					
- 1.3 - 1.3 - Bo 	5.85' - 6.1' vugs $6.1' - 6.4', and 6.7' near hr$ $7.5' core spin$ $9.25' core spin$ $9.25' - 11.9' near vertical$ $12.2' - 13' undulatory, near$ $14.5' core spin$ $19.8' and 19.9' core spin$ $19.8' and 19.9' core spin$ $23.5' angular fracture, iron$ $0x 2 (25' - 44')$ $27' core break at thin (<1' 29.2' angular fracture with$ $34.4' core spin with abracd$ $34.8' angular fracture; slig$ $39.7' angular fracture; with$ $43.5' and 43.7' angular fracture; with$ $43.5' and 43.7' angular fracture; with$ $51.3' so f material al$ $53.9' - 55.3' irregular, near fracture; iron$	n along core break; horizontal; yellowish brown s orizontal breaks with abraded surfaces (weather fracture with apparent iron staining on surface ar vertical fracture; minor iron-staining staining (yellowed brown); missing core at this b ') zone of fissile limey shale; apparent iron staining iron staining and missing core (?) led surfaces; possible iron staining thly weathered surface thapparent dried mud on fracture surface; possil actures; natural (?) apparent iron staining and some dried mud/clay aks along styloltic surfaces; surfaces don't appea	ed appearances) preak (?) ng ere (?) ple iron staining r (1/8") ar to be weathered but there is some nt iron staining on fracture surfaces;				

Alpha Gaoscience 579 Plank Road FRACTURE LOG Page 2 of 2 Project Number/Name: 11110/Honeoye Palls Location: Moneoye Falls, NY End of the Park, New York 12065 DESCRIPTION Box 4 (63.5*-637) 64:1*17 * multiple breaks and paint matching 73.0*:10° multi seam along irregular horizontal fracture: non stained 73.0*:10° multi seam along irregular horizontal fracture. Box 6 (63.5*:4837) 64:1*17 * multiple breaks and paint matching the fragments Box 6 (102.5*:1227) 98:6* irregular, horizontal fracture: no staining 116:3*:angular fracture; no staining 116:3*:angular fracture; no staining 117:4*:angular fracture; no staining 116:3*:angular fracture; no staining 116:3*:angular fracture; no staining 117:4*:angular fracture; no staining 116:1*:0********************************				Boring ID. DDH 4-98				
ALPHA GEOSCIENCE Clifton Park, New York 12065 Page 2 of 2 Project Number/Name: 11110/Honeoye Falls Location: Honeoye Falls, NY Image: Construct of the second s		Alpha Geoscience		Doning ID. DDir 4.00				
Project Number/Name: 11110/Honeoye Falls Project Number/Name: 11110/Honeoye Falls DESCRIPTION Box 4 (63.5' - 83') 64.1' - 1" section of a vertical fracture; iron stained 71' - 71.7' - multiple breaks along chert and stylolites, with iron staining 73.0' - 1/8'' mud seam along irregular horizontal fracture 76.1' - 0.1' thick, dried mud seam with rock fragments Box 5 (83' - 102.5') 99.6' irregular, horizontal fracture; ino staining 115.1' - 115.4' angular fracture; no staining 116.3' angular fracture; no staining 117.4' angular fracture; no staining 120' - 121' rock is fractured, but core is jumbled; flat surfaces 115-121': flat surface - possibly a broken, healed fracture (missing other side)			FRACTURE LOG					
End (f) DESCRIPTION Box 4 (63.5' - 83') 64.1' - 1" section of a vertical fracture; iron stained 71' - 71.7' - multiple breaks along chert and stylolites, with iron staining 73.0' - 1/8" mud seam along irregular horizontal fracture 76.1' - 0.1' thick, dried mud seam with rock fragments Box 5 (83' - 102.5') 99.6' irregular, horizontal fracture; no staining 116.3' angular fracture; no staining 117.4' angular fracture; no staining 120' - 121' rock is fractured, but core is jumbled; flat surfaces flat surfaces; these angular fractures are not along stylolites and appear similar to what is seen in high wall western part of quarry. 121' - 121.6' vertical fracture with minor staining and mineralization on surface - possibly a broken, healed fracture (missing other side)	GEOSCIEN	CE Clifton Park, New York 12065		Page 2 of 2				
Box 4 (63.5' - 83') 64.1' - 1" section of a vertical fracture; iron stained 71' - 71.7' - multiple breaks along chert and stylolites, with iron staining 73.0' - 1/8" mud seam along irregular horizontal fracture 76.1' - 0.1' thick, dried mud seam with rock fragments Box 5 (83' - 102.5') 99.6' irregular, horizontal fracture with dried mud seam Box 6 (102.5' - 122') 115.1' - 115.4' angular fracture; no staining 116.3' angular fracture; no staining 117.4' angular fracture; no staining 120' - 121' rock is fractured, but core is jumbled; flat surfaces 121' - 121.6' vertical fracture with minor staining and mineralization on surface - possibly a broken, healed fracture (missing other side)	Project Nu	umber/Name: 11110/Honeoye Falls	Location: Honeoye Falls, N	Y				
Box 4 (63.5' - 83') 64.1' - 1" section of a vertical fracture; iron stained 71' - 71.7' - multiple breaks along chert and stylolites, with iron staining 73.0' - 1/8" mud seam along irregular horizontal fracture 76.1' - 0.1' thick, dried mud seam with rock fragments Box 5 (83' - 102.5') 99.6' irregular, horizontal fracture with dried mud seam Box 6 (102.5' - 122') 115.1' - 115.4' angular fracture; no staining 116.3' angular fracture; no staining 117.4' angular fracture; no staining 120' - 121' rock is fractured, but core is jumbled; flat surfaces 121' - 121.6' vertical fracture with minor staining and mineralization on surface - possibly a broken, healed fracture (missing other side)	Depth (Ft)		DESCRIPTION					
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Box 7 (122' - 125') many angular fractures; fresh appearing; very flat surfaces	B 	Box 6 (102.5' - 122') 115.1' - 115.4' angular fracture; no staining 116.3' angular fracture; no staining 117.4' angular fracture; no staining 120' - 121' rock is fractured, but core is jumbled; flat surfaces 121' - 121.6' vertical fracture with minor staining and mineralization on surface - possibly a broken,						
	-В	iox 7 (122' - 125') many angular fractures; fr	esh appearing; very flat surfaces					
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4	4							
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O	Alpha Geoscience 679 Plank Road	FRACTURE LOG	Boring ID: DDH 5-98			
ALPH GEOSCIEN	A Clifton Park, New York 12065		Page 1 of 1			
Project Number/Name: 11110/ Hanson Honeoye Falls Location: Honeoye Falls, NY						
Drilling	Drilling Contractor/Personnel: NA					
Geologi	st/Inspector: Steve Trader (Fracture	log only) Start	/ h Date: 1998			
Drilling	Equip/Method: NA	Core Diameter: 1 7/	8"			
Samplir	ng Method: Coring	Well	Installed? No			
Elevatio	on/Ground Surface: 713'					
Depth to	o Ground Water from Ground Surfac	e (Date): Not Measured				
REMAR		ractures only - Geology logged separately in 1998 mmon; staining not present on fracture surfaces u				
Depth (Ft)		DESCRIPTION				
	0-5': unconsolidated overburden					
	Box 1 (not logged)					
	Box 2 (25.5' - 45') 29.4' - 31.2' irregular vertical fracture; with apparent reddish brown staining. [rest of box has many stylolite breaks, but no staining or dried mud]					
	Box 3 (45' - 64.5') 49.2' core spin 50.2' - 51.6' irregular, near vertical fracture; minor staining on some of the fracture surface; end of fracture extends into solid core, but is healed with calcite 57.8' - 58.8' same type of fracture as 50.2' - 51.6'					
	 Box 4 (64.5' - 84') 71' - core break along fissile limey shale 73.6' irregular, horizontal fracture with iron staining; lower piece doesn't fit,well with upper piece 86.6' - 86.9' angular fractures, flat surfaces, no apparent staining 94.3' - 94.5' angular fractures, flat surfaces, no apparent staining 94.8' - 95.1' angular fractures, flat surfaces, no apparent staining 101.4' core spin 					
_	Box 5 (84' - 123') No apparent fractures - did not log the Akron (below 112.5')					
	-					
-						
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	4					
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_						

APPENDIX C

Logs for Expansion Area Monitoring Wells

NEW YORK STATE DEPARTMENT OF ENVIRONMENTAL CON

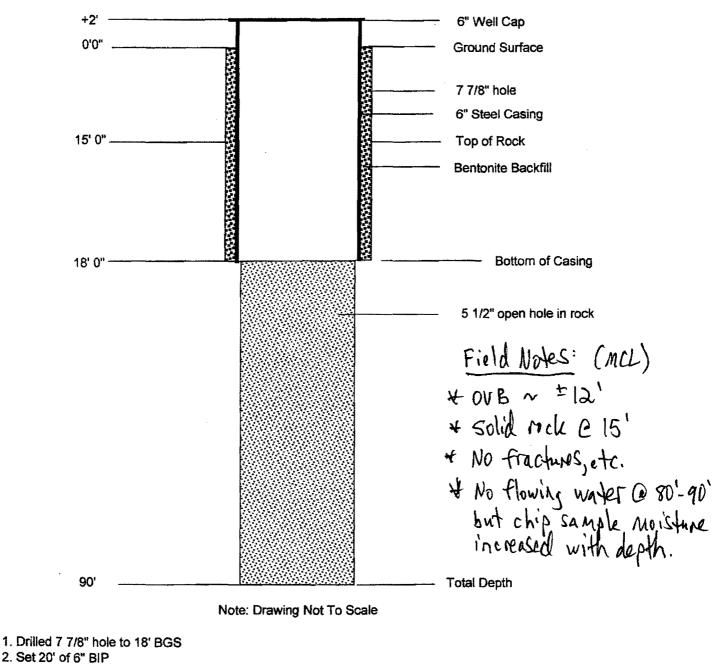
09-001

Honeoye Falls	WATER WELL COMPLETION DEDOOT	mo 1746
4) OWNER	WATER WELL COMPLETION REPORT	
HANSEN Agg-		(Hai LOG
5, ADDRESS	<u>equires</u>	Depth to Bedrock (fr. betc
P.O Box 151, H	oneoye Falls NY 14472	ground surfa
a) LOCATION OF WELL (See Instructions On Reverse) now Lat/Long if available	(Check here if same as address above, also provide Lat / Long below)	Ground Elev (ft. above S
		Top of Casing (ft., above
	56 .721 W 677 38.295 18) DEPTH TO GROUNDWATER DATE MEASURED	or below (-) ground sur
LAND SURFACE (feer) 90	BELOW LAND SURFACE (feet) N.A.	+2 TOR OF WELL
DIAMETER	CASINGS	
6 in	in in	2 Junt - Del
	ft ft ft in	Deve (
SROUT TYPE / SEALING	(12) GROUT / SEALING INTERVAL	YI IA
Bendonite	(feet) FROM TO	
OIMARE & MATERIAL	SCREENS (14) OPENINGS	Topk 4 13
		011-111 1.0-
5-DIAMETER	in in in	Botton of the 10
б) LENGTH		
ft.	ft. ft. m.	
". DEPTH TO TOP OF SCREEN, FROM TOP OF CASING	2 El contra de la co	
	(FP/5))	
	YIELD TEST	
181 DATE		
181 DATE /0-1-0-9 201 LIFT METHOD	YIELD TEST	
18) DATE /0-1-09 20) LIFT METHOD Pump Arr Lift Bail	YIELD TEST (19) DURATION OF TEST (21) STABILIZED DISCHARGE (GPM)	
181 DATE /0-1-0-9 201 LIFT METHOD	YIELD TEST	
	YIELD TEST (19) DURATION OF TEST (21) STABILIZED DISCHARGE (GPM) (23) MAXIMUM DRAWDOWN (Stabilized) (feet/inches below top of casing) (25) Was the water produced during the lest	
18) DATE /O - / - O 9 20) LIFT METHOD Pump Air Lift Bail 25) STATIC LEVEL PRIOR TO TEST (faet/inches below top of casing) 24) RECOVERY (Time in hours/minutes)	YIELD TEST (19) DURATION OF TEST (21) STABILIZED DISCHARGE (GPM) (23) MAXIMUM DRAWDOWN (Stabilized) (feet/inches below top of casing) (25) Was the water produced during the lest discharged away from immediate area	D fort an
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ISI DATE IO - 1 - O 9 INT METHOD Pump Air Lift Bail ISI STATIC LEVEL PRICIP TO TEST (fbef/inches below top of casing) AN RECOVERY (Time in hours/iminutes) Co. PUMP INSTALLED? YESNO	YIELD TEST (19) DURATION OF TEST (21) STABILIZED DISCHARGE (GPM) (23) MAXIMUM DRAWDOWN (Stabilized) (feet/inches below top of casing) (25) Was the water produced during the test discharged (way from immediate area in terring) (25) Was the water produced during the test discharged (way from immediate area in terring) (27) DATE (28) PUMP INSTALLER (29) PUMP INSTALLER	Bottom of
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IBI DATE ID - 1 - 0 9 ID LIFT METHOD Pump ArcLift Bail ID (STATIC LEVEL PRICIP TO TEST (foel/inches below top of casing) PUI ArcCOVERY (Time in hours/minutes) PUI C. PUMP INSTALLED? YESNO PUI ArcCovERY (COMP INSTALLED? YESNO PUI C. PUMP INSTALLED? YESNO PUI C. PUMP INSTALLED? YESNO PUM C. PUMP INSTALLED? YESNO PUMP	YIELD TEST (19) DURATION OF TEST (21) STABILIZED DISCHARGE (GPM) (23) MAXIMUM DRAWDOWN (Stabilized) (feet/inches below top of casing) (25) Was the water produced during the test discharged (way from immediate area interimediate area interinterimedia	Bottom of 70- bott
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Hansen, Honeoye Falls Observation Well Monroe County, NY

<u>09-001</u>

ND Job #3312-09



- 3. Poured Bentonite chips around casing
- 4. Drilled 5 1/2" hole in shale rock to 90' BGS
- Note: Grab samples of rock cuttings were taken by Hansen Representative. Well dnilled dry.

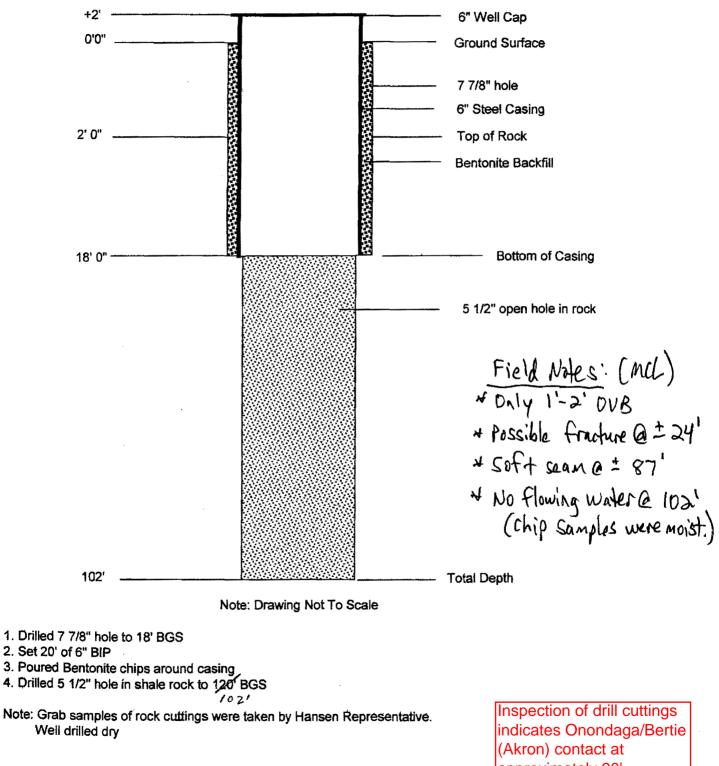
Inspection of drill cuttings indicates Onondaga/ Bertie (Akron) contact at approximately 85' Alpha Geoscience, 2011

	STATE DEPARTMENT	OF ENVIRONMENTAL CON	09-002
NEW TORK			ISERVATION
(1) COUNTY Monroe			(3) DEC Well Number
10			MO 1747
(4) OWNER	ATER WELL CO	OMPLETION REPOR	RT
thansen Acc.	escter.		(43) LOG
(5) ADDRESS		/	Depth to Bedrock (fl. below
P.O. Dox 157		ulls, NY 1447	ground surfac
(6) LOCATION OF WELL (See Instructions On Reverse) Show Lat/Long if available and method used	Check here I if same as add	dress above, also provide Lat / Long be	Ground Elev (it. above S.
	6.604 W	072° 38.522-	Top of Casing (fl., above or below (-) ground surfa
(7) DEPTH OF WELL BELOW LAND SURFACE (feet)	(8) DEPTH TO GROUNDW BELOW LAND SURFA		TOP OF WELL
102	CASINGS	TONE	
(9) DIAMETER	in.	in.	$70R \left(-\frac{1}{2}\right)^2$
(10) LENGTH 20 ft.	ft.	ft, l	Bentenar
	(12) GROUT / SEALING IN	ITERVAL	- seal (
Bentonite	SCREENS	FROM () TO (8	
(13) MAKE & MATERIAL	(14) OPENINGS		- Casing - 1-18
15) DIAMETER			
(16) LENGTH	in.	in. in	<u>۲</u>
ft.	ft.	ft. in	
(17) DEPTH TO TOP OF SCREEN, FROM TOP OF CASING (F	[:] eet)		
	YIELD TEST		
(18) DATE 10-1-09	(19) DURATION OF TEST	A	
(20) LIFT METHOD	(21) STABILIZED DISCHAR	RGE (GPM)	
(22) STATIC LEVEL PRIOR TO TEST	(23) MAXIMUM DRAWDOV		
(feet/inches below top of casing)	(feet/inches below top (25) Was the water produce	-	
	discharged away from	mmediale area? Yes No	
(26) PUMP INSTALLED?	(27) DATE	(28) PUMP INSTALLER	
YES NO	(30) MAKE	(31) MODEL	
		· · · · · · · · · · · · · · · · · · ·	
(32) MAXIMUM CAPACITY (GPM)	(33) PUMP INSTALLATION FROM TOP OF CASIN		
(34: METHOD OF DRILLING	(35) USE OF WATER		
A Rotary Cable Tool Other	(See instructions for cr	_ ODSTRUM I ION WE	2//
(36) DATE DRILLING WORK STARTED $10 - 1 - 0 S$			
(38) DATE REPORT FILED (39) REGISTERED COMPANY		(40) DEC REGISTRATION NO	
10-2-09 Nothnash	e Vrilling 1	WRD 10072	<u> </u>
(41) CERTIFIED DRILLER (Print name)	(42) CERTIFIED DRILLER		ρ
Timothy M Nothing L	e Finit	m Milling	- 102
* By signing this pocument I hereby affirm that. defined by Environmental Conservation Law §15	5-1502: (2) this water well v	was constructed in accordance wit	BOTTOM OF HOLE
water well standards promulgated by the New Y perjury the information provided in this Well Cor understand that any false statement made here	fork State Department of He moletion Poport is true, accurate	alth; (3) under the penalty of	NYSDEC COPY

Hansen, Honeoye Falls Observation Well Monroe County, NY



ND Job #3312-09



approximately 90' Alpha Geoscience, 2011

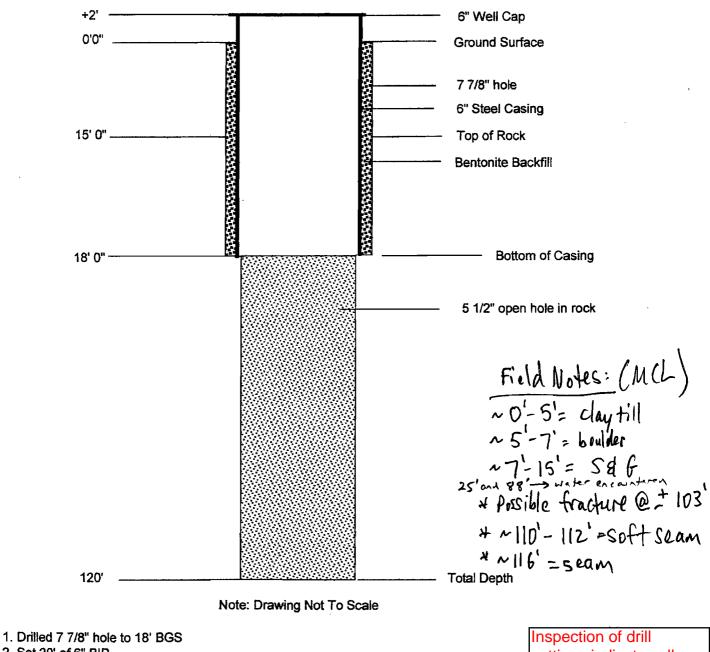
NEW YORK STA	ATE DEPARTMENT	OF ENVIRONMENTAL C	ONSERVATI	ON 09-003
1) COUNTY MONTOL 2) TOWN Honeoye Fulls				(3) DEC Well Number
2) TOWN Honeoye Fulls			ORT	MO 1748
(4) OWNER		OWFLETION REF		
HANSEN Aggrega	tes.			⁽⁴³⁾ LOG
15, ADDRESS PO BOX 151 F	toneoye	Falls NY 1	4472 Dep	h to Bedrock <u>15</u> (ft. below ground surfac
Show Lat/Long if available		dress above, also provide Lat / Lo	- 0100	Ind Elev (ft. above S.)
S GPS Map Interpolation N 4 2 56	·513 W	077 38.842		or below (-) ground surfa
7) DEPTH OF WELL BELOW LAND SURFACE (feet)	(8) DEPTH TO GROUND BELOW LAND SURF	WATER DATE ME	ASURED	TOP OF WELL
	ASINGS	25		H
9) DIAMETER	in.	in.	in.	E 3
(10) LENGTH 20 ft.	ft.	ft.	in.	
11) GROUT TYPE SEALING	(12) GROUT / SEALING (feet)	·		TRA 15
Bentonite	CREENS			31715
13) MAKE & MATERIAL	(14) OPENINGS		(A	5/NG 34 18
15) DIAMETER		·		
in. 16) LENGTH	in.	in.	in	
ft.	ft.	ft.)	in.	
(7) DEPTH TO TOP OF SCREEN, FROM TOP OF CASING (Feet)				
YIE	LD TEST			
	(19) DURATION OF TES			
20) LIFT METHOD	(21) STABILIZED DISCH	ARGE (GPM)		
Pump Arai Lilt Bail	2			
(feet/inches below top of casing)	(23) MAXIMUM DRAWD((feet/inches below to			
24) RECOVERY (Time in hours/minutes)	(25) Was the water produ discharged away from			
PUMP II	NSTALLATION			
26) PUMP INSTALLED? YES NO	(27) DATE	(28) PUMP INSTALLER		
(29) TYPE	(30) MAKE	(31) MODEL		
(12) MAXIMUM CAPACITY (GPM)	(33) PUMP INSTALLATIO FROM TOF OF CAS			
34) METHOD OF DRILLING	(35) USE OF WATER (See instructions for	choices) Observation la)e//	
361 DATE DRILLING WORK STARTED	:37) DATE DRILLING WO	DRK COMPLETED		
(38) DATE REPORT FILED (39) REGISTERED COMPANY	· ·	(40) DEC REGISTRATION N	-	
10-2-09 Nichunagle	142) CERTIFIED DRILLE	NYRD /007	<u>`</u> ~	
Timothy M Nothnasle	(42) GERTIFIEU DRILLE	(m. M. Hung	.C	-120
* By signing this document I hereby affirm that: (1) defined by Environmental Conservation Law \$15-15	02: (2) this water wel	rvise water well drilling activit Il was constructed in accordan	ice with	BOTTOM OF HOLE
water well standards promulgated by the New York perjury the information provided in this Well Comple understand that any false statement made herein is 6210.45	State Department of A	Health; (3) under the penalty	of	NYSDEC COPY

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Hansen, Honeoye Falls Observation Well Monroe County, NY

<u>09-003</u>

ND Job #3312-09



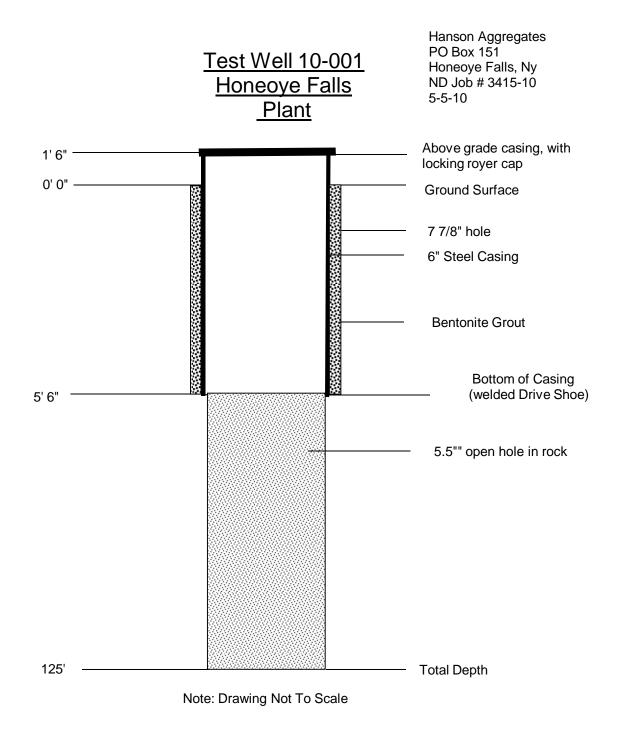
- 2. Set 20' of 6" BIP
- 3. Poured Bentonite chips around casing

4. Drilled 5 1/2" hole in shale rock to 120' BGS

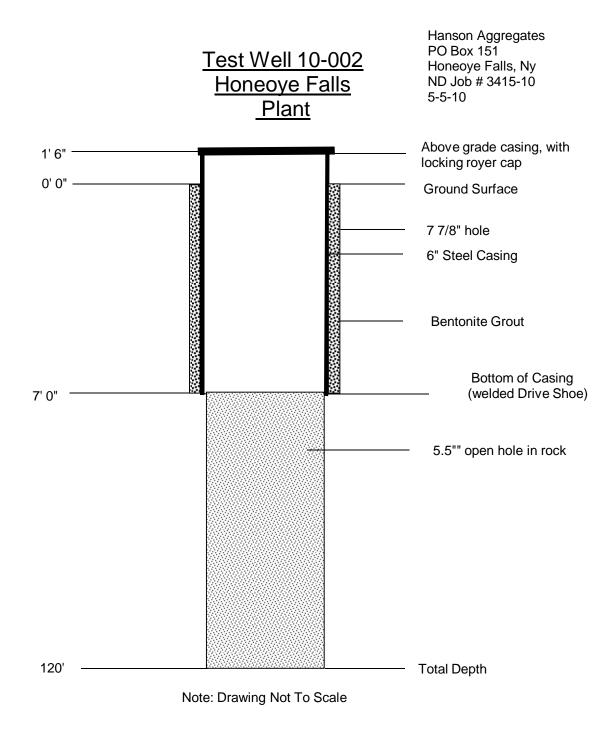
Note: Grab samples of rock cuttings were taken by Hansen Representative.

Encountered water at 25' & 88' BGS, approximately 2 GPM in total.

Inspection of drill cuttings indicates all Onondaga. No Bertie (Akron) encountered. Alpha Geoscience, 2011



NOTE: 1. Encountered water zone at 65' BGS 2. Took grab sample of cuttings, every 5' from 100' to 125' BGS



NOTE: 1. Encountered water zone at 15' BGS 2. Took grab sample of cuttings, every 5' from 95' to 120' BGS

APPENDIX D

Piezometer P1 Well Construction and Geologic Logs

MONITORING WELL COMPLETION LOG



679 Plank Road Clifton Park, New York (518) 348-6995

Well	P1
Project	Hanson-Honeoye Falls
Project No.	11110
Client	Hanson
Date Drilled	4/20/11
Date Develo	ped4/20/11

WELL CONSTRUCTION DETAILS

INSPECTION NOTES

	DEPTH			
		Geologist Matt Dupee		
M.P. EL. <u>703.11</u> — 36"		Drilling Contractor		
		Type of Well Piezometer		
		Static Water Level Date		
700.11	0"	Measuring Point Top PVC		
		Total Well Depth68" (32" below grade)		
	1"			
		Riser Pipe		
		Material PVC Diameter 1"		
1000		Length 50" Joint Type Threaded		
6" Diameter		<u>Screen</u>		
Borehole		Material <u>PVC</u> Diameter <u>1"</u>		
		Slot Size002 in Length18"		
		Stratigraphic Unit Screened Silt & Clay		
	14"			
0 Grade Sand Pack		Packing		
		Sand 0 Gravel Natural Amount 0.4 ft ³ Interval 9"-32"		
		Amount <u>0.4 ft³</u> Interval <u>9"-32"</u>		
Slotted PVC Screen		Seal		
		Type Bentonite Chips Interval 1"-9"		
		Locking Case: Yes No X		
		Diameter		
		Notes:		
	32"			
NOT TO S	DUALE			

11110-Hanson Honeoye Falls Expansion/P1 Completion Log.cvx

Alpha Geoscience 679 Plank Road Clifton Park, New York 12065				Boring ID: P1 Page 1 of 1	
Project Number/Name: 11110 - Hanson Honeoye Falls Expansion Location: Honeoye Falls, NY					
Drilling Contrac	tor/Personnel: Hanson / Lar	ry Clark			
Geologist/Hydro	ogeologist: Matt Dupee		Start Finis	/ h Date: 4/20/2011	
Drilling Equip/M	lethod: Power Auger	Size/Type	of Bit:	6" Auger	
Sampling Meth	od: Drilling Cuttings		Well	Installed? Yes	
Elevation/Grou	nd Surface: 703.11				
Depth to Groun	d Water from Ground Surfac	e (Date):			
REMARKS:					
Depth (in) Sample No.	C	ESCRIPTION		REMARKS	
-		& Silt, trace organics, , moist, medium soft 5"			
6 – – – 12–– – 18 – – 18 – – 24–– –	occasional limest	& Silt to Silt & Clay, one cobbles up to 6", , moist, medium soft. 28'			
30 —		20 Clay, occasional limestone medium to low plasticity, wet, 32"	~28	' - Significant water inflow	
		tom of Boring	32"-	Refusal	
	Proportions Used: Tr	ace=0-10% Little=10-20% Some=20-3	5% And-3	5-50%	